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DEVELOPMENT OF AN AIRCRAFT MANEUVER
LOAD SPECTRUM BASED ON VGH DATA

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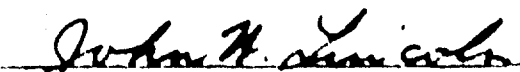
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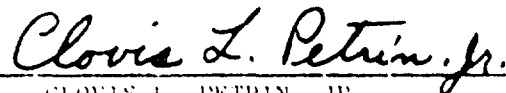
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| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report describes a procedure whereby a full scale aircraft maneuver load fatigue spectrum can be developed from recorded VGH data. It is assumed in this development that the internal loads (stresses) at the appropriate control points are available for combinations of velocity, load factor, altitudes and weight so that an interpolation on these points will provide the desired accuracy. The procedure will generate (for a control point) the cumulative probability of exceeding a given stress, exceedances per hour of a given | | |

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stress level, the probability density function for stress and the stress spectrum. The aircraft spectrum is derived from the assumption that the aircraft test loads derived from a linear combination of balanced loading conditions will provide a good simulation of the stress history at and "between" the control points. The application of the program to new designs (mission analysis) and to tracking can be made without modification. The computer program for this calculation is included along with a sample problem. As an example of an application of this program, the stress exceedance functions for a control point on the wing of the F-4 are shown that were computed from the VGH data accumulated over a period of one year.

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FOREWARD

This report was prepared by John W. Lincoln, Structures Division of the Directorate of Flight Systems Engineering. The work was done as a research and development task to assist in the spectrum development work for the F-4 durability and damage tolerance assessment.

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LIST OF SYMBOLS

| | |
|------------|---|
| N_{vi} | The number of indicated airspeed intervals in the VGH histogram |
| N_{nz} | The number of normal load factor intervals in the VGH histogram |
| N_h | The number of altitude intervals in the VGH histogram |
| N_w | The number of weight intervals in the VGH histogram |
| v_{ii} | Indicated airspeed for the VGH histogram intervals |
| n_{zi} | Normal load factor for the VGH histogram intervals |
| h_i | Altitude for the VGH histogram intervals |
| w_i | Aircraft weight for the VGH histogram intervals |
| H_j | The VGH histogram |
| N_t | The total number of load occurrences in the VGH histogram |
| P_j | The joint probability density function derived from the VGH histogram |
| N_{vi}^R | The number of intervals in a refinement of an indicated airspeed interval in the VGH histogram |
| N_{nz}^R | The number of intervals in a refinement of a normal load factor interval in the VGH histogram |
| N_h^R | The number of intervals in a refinement of an altitude interval in the VGH histogram |
| N_w^R | The number of intervals in a refinement of a weight interval in the VGH histogram |
| V_i | A surface, the ordinates of which are indicated airspeeds for determining the stress at a control point |
| N_z | A surface, the ordinates of which are normal load factors for determining the stress at a control point |

| | |
|------------------|---|
| H | A surface, the ordinates of which are altitudes for determining the stress at a control point |
| W | A surface, the ordinates of which are weights for determining the stress at a control point |
| \hat{P}_J | The joint probability density function for the refined VGH histogram |
| N_p | The number of control points on the aircraft structure used in the derivation of the fatigue spectrum |
| P_{ψ}^a | The cumulative probability for the stress at the ath control point |
| $P_{D_{\psi}}^a$ | The probability density function for the stress at the ath control point |
| A_{cb}^a | The stress for the ath load level at the bth point in the sky and the cth control point |
| Γ_c^a | The fatigue test stress for the ath load level and the cth control point |
| α^{ab} | Scaling coefficients for the ath load level and the bth point in the sky |
| ϕ^a | A surface (generated from the surface P_J) from which P_{ψ}^a can be determined for ath control point |
| ψ^a | The stress surface for the ath control point |
| S^a | A set of ordinates of the graph 1 - P_{ψ}^a |
| $S^a(i)$ | The ith member of S^a |

SECTION I

INTRODUCTION

In the application of the mission analysis required by MIL-A-008866A (USAF) to fighter and attack aircraft a problem arises in the selection of the point in the sky (velocity, altitude, and weight) for the load factor spectrum for the combat segment of the mission. It can be shown that in many cases important differences in the spectrum can be obtained from two "reasonable" point selections.

The problem has been particularly severe on some existing aircraft in that a ten percent shift in the stress spectrum can produce a factor of two change in life. Therefore, when it is considered that essentially all of the fatigue damage for fighter and attack aircraft is done in the combat segment, this part of the mission deserves special attention.

From an examination of available VGH data, it is evident that in both the air-to-air and air-to-ground operations a fairly wide variation in velocity, altitude, and weight is observed. Therefore, it would be surprising if a single point in the sky would provide an accurate prediction of the stress spectrum for a control point. This is even more evident for those aircraft which experience nonlinearities in the aerodynamic data (i.e., tip stall).

One possible solution is to use multiple points in the sky for this calculation. This can be effectively accomplished by taking the points in the sky and their relative frequency of occurrence that are obtained from that portion of the fleet that is equipped with multichannel recorders (twenty percent of the fleet, which is consistent with current policy, is believed to be an adequate sample). This can be done by taking the VGH histogram (the relative frequency of airspeed, normal load factor, altitude, and weight) and dividing by the total number of load occurrences to obtain the probability that a load will occur in a given interval of airspeed, normal load factor, altitude, and weight. A stress level is selected and a summation is made for each such probability where the corresponding stress at the midpoint of the interval of airspeed, etc, is greater than the selected stress level. This computation produces the cumulative probability of exceeding a stress level. Since the intervals used for the data collection were not designed for this calculation, a provision is made to subdivide the intervals to improve the accuracy of the calculation. This technique is explained in Section III. From the cumulative

probability, the number of stress exceedances per hour, the probability density function, and the stress spectrum can be obtained.

Having the functions referred to above for a number of control points that is adequate to cover the aircraft structure (this number may have to be obtained by trial and error), one may generate the full scale aircraft spectrum by assuming that an arbitrary loading at the control points of the structure can be derived from a linear combination of the loading imposed by balanced load conditions. If N_p control points are used, then N_p balanced load conditions are used to represent the control point load. The use of "representative" balanced load conditions should provide a satisfactory interpolation between control points. These intermediate points should be spot checked against the true spectrum to see if the control point coverage is adequate.

Of course, for a new design, the VGH data does not exist and consequently direct application of this method is impossible. In some cases it will be possible to overcome this difficulty by taking existing VGH data from older aircraft and by use of judgement adapt it to this procedure. In any event, the method should be applied when the proper data becomes available so that by suitable tests and analysis the appropriate changes may be made in the aircraft life predictions.

One important application of this procedure is fighter/attack tracking. The unusual technique is to use the fleet counting accelerometer data and compute the stress for a single point in the sky that is believed to be representative of the particular mission flown (i.e., air-to-air or air-to-ground). In lieu of this approach, one could compute from the VGH data the conditional probability of exceeding a stress given the normal load factor. If this function were available, it would be possible to track to any desired probability on even multiple probability levels depending on what results are desired. This function can be generated from this program by setting all occurrences equal to zero except those that fall in the desired load factor interval. The high positive and low negative load factors may require an extrapolation from neighboring load factors because there may be too few data points to adequately describe these functions.

The program that is discussed in this report is based on the load occurrences in the VGH histogram being dependent on indicated airspeed, normal load factor, altitude, and weight. The stress function is based on the same quantities. An immediate alternate that is

included is to use equivalent load factor instead of load factor. This removes the weight dependency and considerably reduces the magnitude of the input. This option is included in the computer program described in the text. Other alternates that could be obtained by a simple modification of the program are listed as follows:

| VGH data based on | Stress function based on |
|--|---|
| 1. Indicated airspeed, normal load factor, altitude, and weight. | Mach no., normal load factor, altitude, and weight. |
| 2. Mach no., normal load factor, altitude, and weight. | Mach no., normal load factor, altitude, and weight. |
| 3. Equivalent airspeed, normal load factor, and weight | Equivalent airspeed, normal load factor, and weight. |

The extension of this program to include other degrees of freedom for the aircraft is immediately evident. The major difficulty is the management of the input data required for the load occurrences and the stress function.

SECTION II

ANALYTICAL DERIVATION OF THE SPECTRUM

The first step in the derivation of the fatigue spectrum is to solve for the stress probability distribution function. This requires that the histogram of occurrences in intervals of indicated airspeed, load factor, altitude, and weight be defined. To do this suppose that each of N_{vi} , N_{nz} , N_h , and N_w is a positive integer and

- (1) v_{ij} is a simple graph such that the x-projection of v_{ij} is the set of integers in $[1, N_{vi} + 1]$ and if i is an integer in $[1, N_{vi} + 1]$ and $i + 1$ is in $[1, N_{vi} + 1]$ then the indicated airspeed $v_{ij}(i)$ is less than the indicated airspeed $v_{ij}(i + 1)$
- (2) n_{zi} is a simple graph such that the x-projection of n_{zi} is the set of integers in $[1, N_{nz} + 1]$ and if j is an integer in $[1, N_{nz} + 1]$ and $j + 1$ is in $[1, N_{nz} + 1]$ then the normal load factor $n_{zi}(j)$, is less than the normal load factor $n_{zi}(j + 1)$
- (3) h_i is a simple graph such that the x-projection of h_i is the set of integers in $[1, N_h + 1]$ and if k is an integer in $[1, N_h + 1]$ and $k + 1$ is in $[1, N_h + 1]$ then the altitude $h_i(k)$, is less than the altitude $h_i(k + 1)$
- (4) w_i is a simple graph such that the x-projection of w_i is the set of integers in $[1, N_w + 1]$ and if m is an integer in $[1, N_w + 1]$ and $m + 1$ is in $[1, N_w + 1]$ the weight $w_i(m)$, is less than the weight $w_i(m + 1)$

Further, suppose H_j is a simple surface such that

$[v_{ij}(i), n_{z_i}(j), h_i(k), w_i(m), H_j(v_{ij}(i), n_{z_i}(j), h_i(k), w_i(m)))]$ is a point of H_j only if

- (1) i is in $[1, N_{v_i}]$, j is in $[1, N_{n_z}]$, k is in $[1, N_h]$,
 m is in $[1, N_w]$ and
- (2) $H_j(v_{ij}(i), n_{z_i}(j), h_i(k), w_i(m))$ is the number of "load occurrences" in the rectangular interval $[v_{ij}(i), v_{ij}(i+1); n_{z_i}(j), n_{z_i}(j+1); h_i(k), h_i(k+1); w_i(m), w_i(m+1)]$ and these load occurrences are assumed to be uniformly distributed within the rectangular interval.

The surface H_j is called the VGH histogram for v_{ij} , n_{z_i} , h_i , and w_i .

The total number of load occurrences included in the VGH histogram H_j is

$$N_t = \sum_{i=1}^{N_{v_i}} \sum_{j=1}^{N_{n_z}} \sum_{k=1}^{N_h} \sum_{m=1}^{N_w} H_j(v_{ij}(i), n_{z_i}(j), h_i(k), w_i(m))$$

Therefore, by definition, the probability that the indicated airspeed, normal load factor, altitude, and weight is in the rectangular interval $[v_{ij}(i), v_{ij}(i+1); n_{z_i}(j), n_{z_i}(j+1);$

$h_i(k), h_i(k+1); w_i(m), w_i(m+1)]$ is

$$P_j(i,j,k,m) = \frac{H_j(v_{ij}(i), n_{z_i}(j), h_i(k), w_i(m))}{N_t}$$

Now suppose that if i is in $[1, N_{V_i} - 1]$ then the interval $[v_{ii}(i), v_{ii}(i + 1)]$ is covered by $N_{V_i}^R$ equal intervals, if j is in $[1, N_{n_z} - 1]$ then $[n_{z_i}(j), n_{z_i}(j + 1)]$ is covered by $N_{n_z}^R$ equal intervals, if k is in $[1, N_h - 1]$ then $[h_i(k), h_i(k + 1)]$ is covered by N_h^R equal intervals, and if m is in $[1, N_w - 1]$ then $[w_i(m), w_i(m + 1)]$ is covered by N_w^R equal intervals.

Since it was supposed that the load occurrences are within the rectangular interval $[v_{ii}(i), v_{ii}(i + 1); n_{z_i}(j), n_{z_i}(j + 1); h_i(k), h_i(k + 1); w_i(m), w_i(m + 1)]$ then the probability that the indicated airspeed, normal load factor, altitude, and weight is in the rectangular interval

$$\begin{aligned} & [v_{ii}(i), v_{ii}(i) + \frac{v_{ii}(i + 1) - v_{ii}(i)}{N_{V_i}^R}; \\ & n_{z_i}(j), n_{z_i}(j) + \frac{n_{z_i}(j + 1) - n_{z_i}(j)}{N_{n_z}^R}; \\ & h_i(k), h_i(k) + \frac{h_i(k + 1) - h_i(k)}{N_h^R}; \\ & w_i(m), w_i(m) + \frac{w_i(m + 1) - w_i(m)}{N_w^R}] \end{aligned}$$

is

$$\hat{P}_J(i, j, k, m) = \frac{H_J(v_i(i), n_z(j), h(k), w(m))}{N_t N_{V_i}^R N_{n_z}^R N_h^R N_w^R}$$

(1) Now suppose that V_i is a simple surface such that the x-y projection of V_i is the set of integers in the rectangular

interval $[1, N_{v_i} + 1; 1, N_{v_i}^R]$ and if i and $i + 1$ are integers

in $[1, N_{v_i} + 1]$ and i_R is an integer in $[1, N_{v_i}^R]$ then

$$v_i(i, i_R) = v_{ii}(i) + \left(\frac{i_R - 0.5}{N_{v_i}^R} \right) (v_{ii}(i + 1) - v_{ii}(i))$$

- (2) N_z is a simple surface such that the x-y projection of N_z is the set of integers in the rectangular interval $[1, N_{n_z} + 1; 1, N_{n_z}^R]$ and if j , and $j + 1$ are integers in

$[1, N_{n_z} + 1]$ and j_R is an integer in $[1, N_{n_z}^R]$ then

$$N_z(j, j_R) = n_{zi}(j) + \left(\frac{j_R - 0.5}{N_{n_z}^R} \right) (n_{zi}(j + 1) - n_{zi}(j))$$

- (3) H is a simple surface such that the x, y projection of H is the set of integers in the rectangular interval $[1, N_h + 1; 1, N_h^R]$ and if k and $k + 1$ are integers in $[1, N_h + 1]$ and

k_R is an integer in $[1, N_h^R]$ then

$$H(k, k_R) = h_i(k) + \left(\frac{k_R - 0.5}{N_h^R} \right) (h_i(k + 1) - h_i(k))$$

- (4) W is a simple surface such that the x, y projection of W is the set of integers in the rectangular interval $[1, N_w + 1; 1, N_w^R]$ and if m and $m + 1$ are integers in $[1, N_w + 1]$

and m_R is an integer in $[1, N_w^R]$ then

$$W(m, m_R) = w_i(m) + \left(\frac{m_R - 0.5}{N_w^R} \right) (w_i(m + 1) - w_i(m))$$

The assumption is made that the stress at a point in the structure depends only on the indicated airspeed, normal load factor, altitude and weight. Therefore, if it is supposed that each of a and N_p is a positive integer such that a is in $[1, N_p]$

and ψ^a is a simple surface such that $(V_i(i, i_R), N_z(j, j_R), H(k, k_R), W(m, m_R), \psi^a(V_i(i, i_R), N_z(j, j_R), H(k, k_R), W(m, m_R)))$ is a point of ψ^a only if i is in $[1, N_{V_i} + 1]$, i_R is in $[1, N_{V_i}^R]$, ..., m is in $[1, N_w + 1]$, m_R is in $[1, N_w^R]$ and $\psi^a(V_i(i, i_R), N_z(j, j_R), H(k, k_R), W(m, m_R))$ is the stress for the a th control point corresponding to the indicated airspeed $V_i(i, i_R)$, the normal load factor $N_z(j, j_R)$, the altitude $H(k, k_R)$, and the weight $W(m, m_R)$.

The surfaces ψ^a and \hat{p}_j are used in the calculation of the cumulative probability of exceeding a given stress as follows: Suppose that N_{Γ_L} is a positive integer and Γ_L is a uniformly increasing sequence with x-projection $[1, N_{\Gamma_L}]$ and ϕ^a is a simple surface such that

- (1) $\phi^a(i, j, k, m, i_R, j_R, k_R, m_R) = \hat{p}_j(i, j, k, m)$
if $\psi^a(V_i(i, i_R), N_z(j, j_R), H(k, k_R), W(m, m_R)) > \Gamma_L(b)$
- (2) $\phi^a(i, j, k, m, i_R, j_R, k_R, m_R) = 0$
if $\psi^a(V_i(i, i_R), N_z(j, j_R), H(k, k_R), W(m, m_R)) \leq \Gamma_L(b)$

Therefore, the probability that the stress is greater than $\Gamma_L(b)$ is

$$P_{\psi^a}(\Gamma_L(b)) = \sum_{i=1}^{N_{V_i}} \sum_{j=1}^{N_{n_z}} \sum_{k=1}^{N_h} \sum_{m=1}^{N_w} \sum_{i_R=1}^{N_{V_i}^R} \sum_{j_R=1}^{N_{n_z}^R} \sum_{k_R=1}^{N_h^R} \sum_{m_R=1}^{N_w^R} \phi^a(i, j, k, m, i_R, j_R, k_R, m_R)$$

The probability density function $P_{D_{\psi^a}}$ is the derivative of the cumulative probability function P_{ψ^a} . This derivative is computed as follows: Suppose a is an integer in $[1, N_p]$ and that ζ^a is a simple graph with x-projection the interval $[1, N_{\Gamma_L}]$ such that

- (1) if b is an integer in $[1, N_{\Gamma_L}]$ then $\zeta^a(b) = P_{\psi}a(b)$ and
- (2) if c is a number in $[b, b + 2]$ there exists a u_1, u_2 , and u_3 such that $\zeta^a(c) = u_1 c^2 + u_2 c + u_3$ where u_1, u_2, u_3 are determined from the equations

$$\begin{array}{rcl} \zeta^a(b) & = & b^2 \\ \zeta^a(b+1) & = & (b+1)^2 \\ \zeta^a(b+2) & = & (b+2)^2 \end{array} \quad \begin{array}{ccc} b & 1 & u_1 \\ (b+1) & 1 & u_2 \\ (b+2) & 1 & u_3 \end{array}$$

Therefore

- (1) if $b = 1$

$$P_{D_{\psi}a}(1) = 2u_1 \Gamma_L(1) + u_2$$

$$P_{D_{\psi}a}(2) = 2u_1 \Gamma_L(1) + u_2$$

- (2) if b is in $[2, N_{\Gamma_L} - 3]$

$$P_{D_{\psi}a}(b+1) = 2u_1 \Gamma_L(b+1) + u_2$$

- (3) if $b = N_{\Gamma_L} - 2$

$$P_{D_{\psi}a}(N_{\Gamma_L} - 1) = 2u_1 \Gamma_L(N_{\Gamma_L} - 1) + u_2$$

$$P_{D_{\psi}a}(N_{\Gamma_L}) = 2u_1 \Gamma_L(N_{\Gamma_L}) + u_2$$

The next step in the derivation of the fatigue loading spectrum is to determine the stress and the frequency of that stress in the spectrum. This is done by an indirect process as shown below. Suppose that the fatigue test spectrum is to be composed of N cycles at M stress levels. Further, suppose that a is a positive integer in $[1, N_p]$ and S^a is a sequence of M numbers such that $s^a(i)$ and $s^a(j)$ are members of S^a only if $0 < s^a(i) < s^a(j) < 1$ and $i < j$.

Therefore, each member of S^a corresponds to an ordinate of the graph $1-P_\psi a$. The M abscissas corresponding to these M ordinates are defined as the M stress levels of the spectrum for the i th control point. The graph $1-P_\psi a$ is known at N_{r_L} points. Consequently, an approximation to $1-P_\psi a$ must be found in order to compute the spectrum stress levels. Suppose β is a simple graph with x -projection the interval $[r_L(1), r_L(N_{r_L})]$ and if k is in $[1, N_{r_L}]$ then $\beta(r_L(k)) = 1-P_\psi a(r_L(k))$. Further, suppose that if $i-1$, i , and $i+1$ are in $[1, N_{r_L}]$, δ_L is $r_L(k+1) - r_L(k)$, and x is in $[-\delta_L, \delta_L]$ then

$$\beta(x + r_L(k)) = \begin{bmatrix} 1 & \frac{x}{\delta_L} & (\frac{x}{\delta_L})^2 \end{bmatrix} \begin{bmatrix} 0 & 1 & 0 \\ -\frac{1}{2} & 0 & \frac{1}{2} \\ \frac{1}{2} & -1 & \frac{1}{2} \end{bmatrix} \begin{bmatrix} \beta(r_L(k-1)) \\ \beta(r_L(k)) \\ \beta(r_L(k+1)) \end{bmatrix}$$

It follows then that if i is in $[1, M]$ there exists an integer k such that $P_\psi a(r_L(k-1)) \leq s^a(i) \leq P_\psi a(r_L(k))$ and a number x such that $\beta(x + r_L(k)) = s^a(i)$. The number x is obtained from a solution of a quadratic equation and $x + r_L(k)$ is the stress corresponding to $s^a(i)$.

The fraction of the N cycles, n_i , that are associated with the i th stress level is defined as follows:

$$\begin{aligned} n_1 &= \frac{s(1) + s(2)}{2} \\ n_i &= \frac{s(i+1) - s(i-1)}{2} \quad 1 < i < M \\ n_M &= 1 - \frac{(s(M) + s(M-1))}{2} \end{aligned}$$

It follows then that if i is in $[1, M]$ and if the sequence S^a is used for each of the control points then there will be an equal number of loading cycles for the i th load level for each of the control points.

The final step is to determine a set of coefficients which when multiplied by the stresses corresponding to balanced load conditions for the aircraft will produce the desired stress levels at the aircraft control points. Suppose a is a positive integer in $[1, M]$, b is a positive integer in $[1, N_p]$, and c is a positive integer in $[1, N_c]$. Therefore, if A_{cb}^a is the stress for the a th load level at the b th point in the sky and the c th control point and r_c^a is the stress desired in the fatigue test for the a th load level and the c th control point then there exists a set of coefficients α_{ab} such that $r_c^a = \sum_b A_{cb}^a \alpha_{ab}$.

SECTION III

DESCRIPTION OF THE COMPUTER PROGRAM

1 NOTATION

The right hand side of the following relations are defined in Section II.

$$NT421 = N_{v_i}$$

$$NT422 = N_{n_z}$$

$$NT423 = N_h$$

$$NT424 = N_w$$

$$NT = N_t$$

$$PJT = \hat{P}_J$$

$$NRVI = N_{v_i}^R$$

$$NRNZ = N_{n_z}^R$$

$$NRH = N_h^R$$

$$NRW = N_w^R$$

$$VII = v_{ii}$$

$$NZI = n_{z_i}$$

$$HI = h_i$$

$$WI = w_i$$

$$VI = V_i$$

$$NZ = N_z$$

$$H = H$$

$$W = W$$

$$NPS = N_p$$

$$PPSI = P_{\psi} a \text{ (The } a \text{ is not explicitly identified in the program)}$$

$$PDPSI = P_{D_{\psi}} a \text{ (The } a \text{ is not explicitly identified in the program)}$$

$$PS = A$$

$PLD = \Gamma$
 $ALPHA = \alpha$
 $FVI = v_{ii}(N_{v_i} + 1)$
 $FNZ = n_{zi}(N_{n_z} + 1)$
 $FH = h_i(N_h + 1)$
 $FW = w_i(N_w + 1)$
 $FACTØR$ - Stress scaling factor. $FACTØR = 1$ unless otherwise specified.
 $HØURS$ - The number of hours of data in the VGH histogram
 $PSIL = \Gamma_L$
 $AREAN = s^a$
 $DELTA = \delta_L$
 $APDPSI(I) = 1.0 - PPSI(I)$
 $PSILL(I)$ - The stress level that is the abscissa of the point of PPSI whose ordinate is $AREAN(I)$
 $FRAC(I)$ - The fraction of the total number of cycles in the spectrum that correspond to $PSILL$
 $NPSIL = N_{\Gamma_L}$
 $NPSILL = M$
 $EXCEED(I)$ - The number of exceedances per hour of the stress $PSIL(I)$
 $NZERO$ - Control number to zero the input numbers at the start of a run and then prevent them from being zeroed between cases
 $NPSCT$ - Control number for counting the number of control points for which a spectrum has been computed in a single run

2 INTERPOLATION PROCEDURE

Since the stress is initially calculated for only a finite set of points on the stress surface, an assumption must be made to determine the stress for a given indicated airspeed, normal load factor, altitude, and weight. Specifically, the problem may be expressed as follows: Given that $NT421$, $NT422$, $NT423$, $NT424$, $NRVI$, $NRNZ$, NRH , and NRW is a positive integer and I is in $[1, NT421]$, J is in $[1, NT422]$, K is in $[1, NT423]$, M is in $[1, NT424]$, IR is in $[1, NRVI]$, JR is in $[1, NRNZ]$, KR is in $[1, NRH]$, MR is in $[1, NRW]$ and a is in $[1, N_p]$ it is required to create an approximation in the form

$$\xi^a(I, J, K, M, IR, JR, KR, MR) =$$

$$\Xi^a(VI(I, IR), NZ(J, JR), H(K, KR), W(M, MR))$$

for the stress as expressed by

$$\psi^a(I, J, K, M, IR, JR, KR, MR) =$$

$$\Psi^a(VI(I, IR), NZ(J, JR), H(K, KR), W(M, MR))$$

where Ξ^a is a ruled surface based on $2^4 = 16$ points of Ψ^a . The method of choosing these 16 points and the calculation of the stress approximation is described below.

The first step is to define the function TABLE which contains the projections and ordinates of the Ψ^a surface.

Suppose each of NTAB1, NTAB2, NTAB3, and NTAB4 is a positive integer and that

$$NN12 = NTAB1 + NTAB2$$

$$NN13 = NN12 + NTAB3$$

$$NN14 = NN13 + NTAB4$$

$$NP = NTAB1 \cdot NTAB2 \cdot NTAB3 \cdot NTAB4$$

$$NF = NN14 + NP$$

Further, suppose that TABLE is a simple graph such that the x-projection of TABLE is the set of integers in the interval [1, NF] and each of I1, I2, I3, and I4 is a positive integer.

Also,

- (1) if I1 and I1 + 1 are in [1, NTAB1] then the indicated airspeed TABLE (I1) is less than the indicated airspeed TABLE (I1 + 1)
- (2) if I2 and I2 + 1 are in [NTAB1 + 1, NN12] then the normal load factor TABLE (I2) is less than the normal load factor TABLE (I2 + 1)
- (3) if I3 and I3 + 1 are in [NN12 + 1, NN13] then the altitude TABLE (I3), is less than the altitude TABLE (I3 + 1)
- (4) if I4 and I4 + 1 are in [NN13 + 1, NN14] then the weight TABLE (I4) is less than the weight TABLE (I4 + 1)
- (5) if I1 is in [1, NTAB1], I2 is in [NTAB1 + 1, NN12], I3 is in [NN12 + 1, NN13], I4 is in [NN13 + 1, NN14]

and n is in $[NN14 + 1, NF]$ and is equal to $NN14 + (I4 - NN13 - 1) \cdot NTAB3 \cdot NTAB2 \cdot NTAB1 + (I3 - NN12 - 1) \cdot NTAB2 \cdot NTAB1 + (I2 - NTAB1 - 1) \cdot NTAB1 + I1$ then the stress TABLE (n) is the stress that corresponds to the indicated airspeed TABLE ($I1$), the normal load factor TABLE ($I2$), the altitude TABLE ($I3$) and the weight TABLE ($I4$).

The positive integers $I1$, $I2$, $I3$, and $I4$ are determined as follows: A search is made for the integer i that will determine the smallest number TABLE (i) that equals or exceeds $VI(I,IR)$. If $i = 1$ satisfies this requirement then $I1$ is set equal to 2. If i is in $[2, NTAB1]$ then $I1$ is set equal to i . If no i can be found in $[2, NTAB1]$ then $I1$ is set equal to $NTAB1$. A search is made for the integer j that will determine the smallest number TABLE (j) that equals or exceeds $NZ(J,JR)$. If $j = NTAB1 + 1$ then $I2$ is set equal to $NTAB1 + 2$. If j is in $[NTAB1 + 2, NN12]$ then $I2$ is set equal to j . If no j can be found to satisfy the requirement then $I2$ is set equal to $NN12$. Also, a search is made for the integer k that will determine the smallest number TABLE (k) that equals or exceeds $H(K,KR)$. If $k = NN12 + 1$ then $I3$ is set equal to $NN12 + 2$. If k is in $[NN12 + 2, NN13]$ then $I3$ is set equal to k . If no k can be found in $[NN12 + 2, NN13]$ then $I3$ is set equal to $NN13$. A final search is made for the integer m that will determine the smallest number TABLE (m) that equals or exceeds $W(M,MR)$. If $m = NN13 + 1$ then $I4$ is set equal to $NN13 + 2$. If m is in $[NN13 + 2, NN14]$ then $I4$ is set equal to m . If no m can be in $[NN13 + 2, NN14]$ then $I4$ is set equal to $NN14$.

The next step is to identify the integers required for the final calculations.

With

$$\begin{aligned} NP12 &= NTAB1 \cdot NTAB2 \\ NP13 &= NP12 \cdot NTAB3 \end{aligned}$$

these are:

$$\begin{aligned} N2222 &= NN14 + (I4 - NN13 - 1) \cdot NP13 + (I3 - NN12 - 1) \cdot \\ &\quad NP12 + (I2 - NTAB1 - 1) \cdot NTAB1 + I1 \\ N1222 &= N2222 - 1 \\ N2122 &= N2222 - NTAB1 \\ N1122 &= N2122 - 1 \\ N2212 &= N2222 - NP12 \end{aligned}$$

```

N1212 = N2212 - 1
N2112 = N2212 - NTAB1
N1112 = N2112 - 1
N2221 = N222 - NP13
N1221 = N2221 - 1
N2121 = N2221 - NTAB1
N1121 = N2121 - 1
N2211 = N2221 - NP12
N1211 = N2211 - 1
N2111 = N2211 - NTAB1
N1111 = N2111 - 1

```

Therefore, if

$$X1RAT = \frac{VI(I,IR) - TABLE(I1-1)}{TABLE(I1) - TABLE(I1-1)}$$

$$X2RAT = \frac{NZ(J,JR) - TABLE(I2-1)}{TABLE(I2) - TABLE(I2-1)}$$

$$X3RAT = \frac{H(K,KR) - TABLE(I3-1)}{TABLE(I3) - TABLE(I3-1)}$$

$$X4RAT = \frac{W(M,MR) - TABLE(I4-1)}{TABLE(I4) - TABLE(I4-1)}$$

then

```

AMP111 = TABLE(N1111) + X1RAT(TABLE(N2111) - TABLE(N1111))
AMP211 = TABLE(N1211) + X1RAT(TABLE(N2211) - TABLE(N1211))
AMP121 = TABLE(N1121) + X1RAT(TABLE(N2121) - TABLE(N1121))
AMP221 = TABLE(N1221) + X1RAT(TABLE(N2221) - TABLE(N1221))
AMP112 = TABLE(N1112) + X1RAT(TABLE(N2112) - TABLE(N1112))
AMP212 = TABLE(N1212) + X1RAT(TABLE(N2212) - TABLE(N1212))
AMP122 = TABLE(N1122) + X1RAT(TABLE(N2122) - TABLE(N1122))
AMP222 = TABLE(N1222) + X1RAT(TABLE(N2222) - TABLE(N1222)),

```

```

AMP11 = AMP111 + X2RAT(AMP211 - AMP111)
AMP12 = AMP112 + X2RAT(AMP212 - AMP112)
AMP22 = AMP122 + X2RAT(AMP222 - AMP122),

```

```

AMP1 = AMP11 + X3RAT(AMP21 - AMP11)
AMP2 = AMP12 + X3RAT(AMP22 - AMP12),

```

$$\xi^a(K,J,K,M,IR,JR,KR,MR) = (AMP1 + X4RAT(AMP2 - AMP1)) \cdot FACTOR$$

It is seen that the sixteen points on the ψ^a surface are reduced to eight points on the Ξ^a surface by an interpolation on the indicated airspeed. The eight points are reduced to four points on the Ξ^a surface by an interpolation on the normal load factor. Next, the

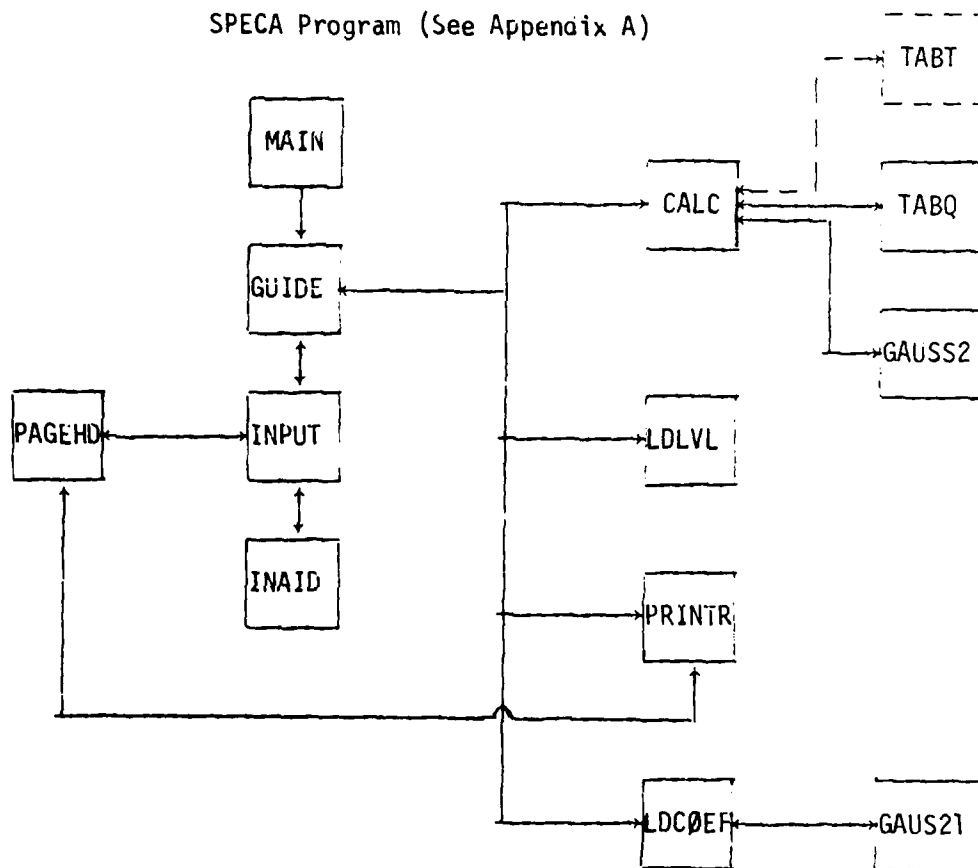
four points are reduced to two points on the Ξ^a surface by an interpolation on the altitude, and finally these two points are reduced to the desired stress by an interpolation on the weight.

Note that the number FACTØR is used to scale the calculation made in the table look up routine.

3 COMPUTER FLOW DIAGRAM AND PROGRAM

The computer routine was coded in FORTRAN Extended Language with the main program and subroutines arranged as follows:

SPECA Program (See Appendix A)



MAIN - Main Program - Sets NZERØ and NPSCT to zero and transfers program control to GUIDE

GUIDE - Subroutine - Initially zeros input and output numbers and after first case zeros output numbers before the calculations are performed. GUIDE, the main controlling subroutine, transfers control to INPUT, CALC, LDLVL, PRINTR, and LDCDEF in turn.

INPUT - Subroutine - Reads in all input data including the VGH histogram and the stress table. There are two formats for reading in floating point numbers and three formats for reading in fixed point numbers. The details of the data input are discussed later in this section.

INAID - Subroutine - Called by INPUT and has the purpose of writing out certain input data.

- (1) NRVI, NRNZ, NRH, NRW
- (2) FACTOR
- (3) PSIL
- (4) AREAN
- (5) PS
- (6) Stress table
- (7) VGH histogram table
- (8) FVI, FNZ, FH, FW

Also, INAID sets NZERO=1 for control of data handling in GUIDE

PAGEHD - Subroutine - Writes out page heading including run identification, date and page number

CALC - Subroutine - Computes PPSI and PDPSI

LDLVL - Subroutine - Computes PSIL and FRAC

LDCDEF - Subroutine - Computer ALPHA

TABQ - Subroutine - Called from CALC to perform the interpolation discussed in Section IV, B, that computes the stress corresponding to a given indicated airspeed, normal load factor, altitude, and weight.

TABT - Subroutine - called from CALC as an alternate to TABQ for the interpolation to compute the stress corresponding to a given indicated airspeed, equivalent normal load factor, and altitude.

GAUSS2 - Subroutine - Called from CALC to solve the simultaneous equations that are required to pass second order equations through the points of PPSI so that the differentiation for PDPSI can be performed. The subroutine uses the Gauss-Jordan method for solving the sets of simultaneous equations.

GAUS21 - Subroutine - Called from LDCDEF and is used to solve the set of equations $PLD(I) = PS(K,J) \cdot ALPHA(J)$. This subroutine is identical to GAUSS2 except for a DIMENSION statement change.

PRINTR - Subroutine - Called from GUIDE to write out computed output data. In particular, PRINTR prints

- (1) PPSI
- (2) EXCEED
- (3) HOURS
- (4) PDPSI
- (5) PSILL, FRAC

4 EQUIVALENCE TABLES

The technique that has been used in coding this routine is to place all input and output numbers in blank common. All input and output floating point numbers are called parameters and are contained in P (dimensioned 10,000). All input and output fixed point numbers are called integers and are contained in NTEGER (dimensioned 100). To make the program more easily interpreted, EQUIVALENCE statements are used to provide the P and NTEGER numbers with more recognizable names. The SPECA program parameter and integer tables are given below.

PARAMETER EQUIVALENCE TABLE

| P | Dimension | Term | P | Dimension | Term |
|---|-----------|---------|------|-----------|--------------|
| 1 | (1) | FMN,FVI | 1201 | (100) | APDPSI(1) |
| 2 | (1) | FNZ | 1300 | | APDPSI(100) |
| 3 | (1) | FH | 1301 | (100) | PSIL(1) |
| 4 | (1) | FW | 1400 | | PSIL(100) |
| 5 | (1) | FACTØR | 1401 | (100) | FRAC(1) |
| 6 | (1) | HØURS | 1500 | | FRAC(100) |
| . | | | 1501 | (100,25) | PLDS(1,1) |
| . | | | 4000 | | PLDS(100,25) |
| . | | | 4001 | (25) | ALPHA(1) |
| . | | | 4025 | | ALPHA(25) |

| P | Dimension | Term | P | Dimension | Term |
|------|-----------|------------|------|-----------|-------------|
| 100 | (1) | NT | . | | |
| 101 | (100) | PSIL(1) | . | | |
| 200 | | PSIL(100) | . | | |
| 201 | (100) | AREAN(1) | 5001 | (25) | VII(1) |
| 300 | | AREAN(100) | 5025 | | VII(25) |
| 301 | (25,25) | PS(1,1) | 5026 | (25) | NZI(1) |
| 925 | | PS(25,25) | 5050 | | NZI(25) |
| . | | | 5051 | (25) | HI(1) |
| . | | | 5075 | | HI(25) |
| . | | | 5076 | (25) | WI(1) |
| 1001 | (100) | PPSI(1) | 5100 | | WI(25) |
| 1100 | | PPSI(100) | . | | |
| 1101 | (100) | PDPSI(1) | . | | |
| 1200 | | PDPSI(100) | 6001 | (100) | EXCEED(1) |
| | | | 6100 | | EXCEED(100) |

INTEGER EQUIVALENCE TABLE

| NTEGER | Dimension | Term | NTEGER | Dimension | Term |
|--------|-----------|--------|--------|-----------|----------|
| 1 | (1) | IDENT | . | | |
| 2 | . | NPF1 | . | | |
| 3 | . | NPF2 | . | | |
| 4 | . | NPF3 | 56 | (2) | NTB41(1) |
| 5 | | NPF4 | 57 | | NTB41(2) |
| 6 | | NTI4 | 58 | (2) | NTB42(1) |
| 7 | | NTW4 | 59 | | NTB42(2) |
| 8 | | MONTH | 60 | (2) | NTB42(1) |
| 9 | | DAY | 61 | | NTB43(2) |
| 10 | | YEAR | 62 | (2) | NTB44(1) |
| 11 | | NPSIL | 63 | | NTB44(2) |
| 12 | | NPSILL | 64 | (1) | NTB21 |
| 13 | | NPS | 65 | (1) | NTB22 |
| 14 | | NMORE | | | |
| 15 | | NRMN | | | |
| 16 | | NRNZ | | | |
| 17 | | NRH | | | |
| 18 | | NRW | | | |
| 19 | | | | | |
| 20 | | | | | |
| 21 | | NTB | | | |
| . | | | | | |
| . | | | | | |
| 49 | | NPAGE | | | |

5 INPUT DATA

All of the input data described below is read into the program by means of the subroutine INPUT. INPUT is a general purpose subroutine for reading data from cards. For this program, the full capabilities of INPUT are not required and consequently there will be some zeros in the input that serve to bypass certain options.

The following deck arrangement is recommended:

1415 Format

| | | | | | | | | | | | | | |
|-------|------|---|---|---|------|------|-------|-----|------|-------|--------|-----|----|
| IDENT | NPF1 | 0 | 0 | 0 | NTI4 | NTW4 | MONTH | DAY | YEAR | NPSIL | NPSILL | NPS | 21 |
|-------|------|---|---|---|------|------|-------|-----|------|-------|--------|-----|----|

715 Format

| | | | | | | |
|------|------|-----|-----|---|---|-----|
| NRVI | NRNZ | NRH | NRW | 0 | 0 | NIB |
|------|------|-----|-----|---|---|-----|

72H Format

| |
|-----------------|
| Run Description |
|-----------------|

72H Format

| |
|-----------------|
| Run Description |
|-----------------|

315

| | | |
|---|---|---|
| 1 | 6 | 1 |
|---|---|---|

6E10.3 Format

| | | | | | |
|-----|-----|----|----|--------|-------|
| FVI | FNZ | FH | FW | FACTØR | HØURS |
|-----|-----|----|----|--------|-------|

315 Format

| | | |
|-----|----------------|---|
| 101 | 100 + NPSIL | 1 |
|-----|----------------|---|

6E10.3 Format

PSIL(1) - PSIL(NPSIL)

315 Format

| | | |
|-----|-----------------|---|
| 201 | 200 + NPSILL | 1 |
|-----|-----------------|---|

6E10.3 Format

AREAN(1) - AREAN(NPSILL)

If NPS > 1 go to (a)

If NPS = 0 go to (b)

(a) 315 Format

| | | |
|-----|-------------|---|
| 301 | 300+ NPS | 1 |
|-----|-------------|---|

6E10.3 Format

PS(1,1) - (PS(NPS,1)

315 Format

| | | |
|-----|--------------|---|
| 326 | 325 + NPS | 1 |
|-----|--------------|---|

6E10.3 Format

PS(1,2) - PS(NPS,2)

3I5 Format

| | | |
|-----|--------------|---|
| 351 | 350 + NPS | 1 |
|-----|--------------|---|

6E10.3 Format

| |
|---------------------|
| PS(1,3) - PS(NPS,3) |
|---------------------|

.
.
.

3I5 Format

| | | |
|------------------------|-----------------------------|---|
| 301 + 25(NPS -1) | 300 + (NPS-1) -25+NPS | 1 |
|------------------------|-----------------------------|---|

6E10.3 Format

| |
|-------------------------|
| PS(1,NPS) - PS(NPS,NPS) |
|-------------------------|

- (b) If NTI4 > 0 go to (c) to read NI14 table(s). For the first run in a computer input the stress table and the VGH histogram table must be read. Subsequent runs may require no new tables (NTI4 = 0), one new table (NTI4 = 1), or two new tables (NTI4 = 2).

If NTI4 = 0 go to (g)

- (c) 5I10 Format

| | | | | |
|---|-------|-------|-------|-------|
| 1 | NTAB1 | NTAB2 | NTAB3 | NTAB4 |
|---|-------|-------|-------|-------|

(Stress table control cards)

6E10.3 Format

TABLE(1) - TABLE(NTAB1)
(indicated airspeeds for the stress table)

6E10.3 Format

TABLE(NTAB1+1) - TABLE(NN12)
(normal load factors for the stress table)

6E10.3 Format

TABLE(NN12+1) - TABLE(NN13)
(altitudes for the stress table)

If NTB = 1 go to (d)

If NTB = 2 go to (e)

(d)

6E10.3 Format

TABLE(NN13+1) - TABLE(NN14)
(weights for the stress table)

6E10.3 Format

TABLE(NN14+1) - TABLE(NF)
(stress amplitudes for the stress table)
(see Section 3.2 for ordering of these entries)

go to (f)

(e)

E10.3 Format

WTTB3
(ref. weight)

6E10.3 Format

TABLE(NN13+1) - TABLE(NF)
(stress amplitudes for the stress table)
(see Section 3.2 for ordering of these entries)

(f)

5I10 Format

| | | | | |
|---|-------|-------|-------|-------|
| 2 | NT421 | NT422 | NT423 | NT424 |
|---|-------|-------|-------|-------|

(VGH histogram control cards)

6E10.3 Format

VII(1) - VII(NT421)
(indicated airspeeds for VGH histogram table)

NZI(1) - NZI(NT422)
(normal load factor for VGH histogram table)

HI(1) - HI(NT423)
(altitudes for VGH histogram table)

WI(1) - WI(NT424)
(weights for VGH histogram table)

$\gamma^a(VII(1), NZI(1), HI(1), WI(1)) -$
 $\gamma^a(VII(NT421), NZI(NT422), HI(NT423), WI(NT424))$
(load occurrences in VGH histogram table)
(see discussion below for ordering of these entries)

(g) END OF FILE

The first card contains 14 fixed point (integer) numbers arranged in 15 fields. These 14 entries in order on this card are

- (1) IDENT - run number
- (2) NPF1 = 3 if $N_p = 1$
= 3 + N_p if $N_p > 1$
- (3) 0
- (4) 0
- (5) 0
- (6) NI14 - the number of quadruple tables to be read (for this count the stress table and the VGH histogram table are each considered quadruple tables.)

- (7) NIW4 = 1 for print of quadruple tables
= 0 otherwise
- (8) MONTH - month in date for page heading
- (9) DAY - day in date for page heading
- (10) YEAR - year in date for page heading
- (11) NPSIL = N_{FL}
- (12) NPSILL = N
- (13) NPS - the number of control points if $N_p > 1$. NPS = 0
if $N_p = 1$
- (14) 21

The second card contains seven fixed point numbers arranged in 15 fields. In order these entries are

- (1) NRVI = $N_{v_i}^R$
- (2) NRNZ = $N_{n_z}^R$
- (3) NRH = N_h^R
- (4) NRW = N_w^R
- (5) 0
- (6) 0
- (7) NTB = 1 if the load occurrences in the VGH histogram depend on indicated airspeed, normal load factor, altitude, and weight.
NTB = 2 if the load occurrences in the VGH histogram depend on indicated airspeed, equivalent normal load factor, and altitude

The third and fourth cards contain a 72H field each for the purpose of run description, etc.

The fifth card contains 1, 6, and 1 in 15 fields

The sixth card contains six floating point numbers arranged in E10.3 fields. These six numbers are placed in the following order:

- (1) FVI = $v_i(N_{v_i} + 1)$

$$(2) \quad FNZ = n_z(N_{n_z} + 1)$$

$$(3) \quad FH = h(N_h + 1)$$

$$(4) \quad FW = w(N_w + 1)$$

(5) FACTOR - stress scaling factor

(6) HOURS - number of hours of data in the VGH histogram

The seventh card contains the three fixed point numbers 101, 100 + NPSIL, 1 in order in 15 fields. NPSIL must not exceed 100.

The next card(s) contain(s) the numbers PSIL(1) through PSIL(NPSIL) in E10.3 fields, six numbers per card.

The next entry contains the fixed point numbers 201, 200 + NPSILL, 1 in order in 15 fields. NPSILL must not exceed 100.

Following this card the floating point numbers AREAN(1) through AREAN(NPSIL), arranged in E10.3 fields, six numbers per card, are entered.

If NPS = 0 then the PS matrix is omitted from the input deck.

If NPS = 1 then the PS matrix is placed next in the input deck. PS is dimensioned (25,25) and is equivalenced to P such that $P(301) = PS(1,1)$. Therefore, it follows that $P(300+NPS) = PS(NPS,1)$, $P(326) = PS(1,2)$, and $P(301+25(NPS-1)) = PS(1,NPS)$. Consequently the NPS blocks of data are read in as follows:

First block -

The first card contains the fixed point numbers 301, 300+NPS, 1 arranged in 15 fields.

The next entries are the floating point numbers PS(1,1) through PS(NPS,1) in E10.3 fields, six numbers per card.

Second block -

The first card contains the fixed point numbers 326, 325+NPS, 1 arranged in 15 fields.

The next entries are the floating point numbers $PS(1,2)$ through $PS(NPS,2)$ in E10.3 fields, six numbers per card.

.

NrSth block -

The first card contains the fixed point numbers $301 + 25(NPS-1)$, $300 + (NPS-1)(25) + NPS$ arranged in 15 fields.

The next entries are the floating point numbers $PS(1,NPS)$ through $PS(NPS,NPS)$ in E10.3 fields, six numbers per card.

The remaining entries are the stress table and the VGH histogram table. These entries are prepared as follows:

If $I = 1$ then the entry is the stress table where there are $NP = NTAB1 \cdot NTAB2 \cdot NTAB3 \cdot NTAB4$ points defined by $NTAB1$ indicated airspeeds, $NTAB2$ normal load factors, $NTAB3$ altitudes, $NTAB4$ weights. These points are entered as ordinates of the simple graph TABLE which was defined in paragraph 2 of this section.

The first card for the stress table contains five (5) fixed point numbers in 15 fields in the order:

- (1) 1
- (2) $NTAB1$
- (3) $NTAB2$
- (4) $NTAB3$
- (5) $NTAB4$

The next card(s) contain(s) the indicated airspeeds (floating point numbers) $TABLE(1)$ through $TABLE(NTAB1)$ arranged in E10.6 fields, six numbers per card.

The next entries are the normal load factors $TABLE(NTAB1 + 1, NN12)$ (see paragraph 2 for definition of arguments) arranged in E10.3 fields six numbers per card.

Next, the card(s) that contain the altitudes $TABLE(NN12+1)$ through $TABLE(NN13)$ arranged in E10.3 fields, six numbers per card are entered in order.

The next entries depend on the number NTB.

If NTB = 1 the card(s) that contain(s) the weights TABLE(NN13+1) through TABLE(NN14) arranged in E10.3 fields, are entered with six numbers per card.

The next card(s) contain(s) the stresses TABLE(NN14+1) through TABLE(NF) arranged in E10.3 fields, six numbers per card. The ordering of the stresses in this entry is defined in paragraph 2 of this section.

If NTB = 2 a card is entered that contains the reference weight WTTB3 in an E10.3 field.

The next card(s) contain(s) the stresses TABLE(NN13+1) through TABLE(NF) arranged in E10.3 fields, six numbers per card. The number NF must not exceed 2000. The ordering of the stresses in this entry is defined in paragraph 2 of this section. (Note that NTAB4 = 1 for this case.)

This completes the stress table

If I = 2 then the entry is the VGH histogram table where there are NP24 = NT421 * NT422 * NT423 * NT424 regions defined by NT421 indicated airspeed intervals, NT422 normal load factor intervals, NT423 altitude intervals, and NT424 weight intervals.

The first card for the VGH histogram table contains five fixed point numbers in I5 fields in the order

- (1) 2
- (2) NT421
- (3) NT422
- (4) NT423
- (5) NT424

Following this card are the card(s) with the indicated airspeeds (floating point numbers) VII(1) through VII(NT421) arranged in E10.3 fields, six numbers per card.

The next card(s) contain the normal load factors NZI(1) through NZI(NT422) arranged in E10.3 fields, six numbers per card.

Next are the card(s) that contain the altitudes HI(1) through HI(NT423) arranged in E10.3 fields, six numbers per card.

The weight entries WI(1) through WI(NT424) arranged in E10.3 field, six numbers per card, are next.

The final card(s) in the VGH histogram deck are the load occurrences in regions defined by the indicated airspeeds, normal load factors, altitudes, and weights. If i is in [1, NP] then these entries are $PI(VII(i), NZI(1), HI(1), WI(1))$ through $PI(VII(NT421), NZI(NT422), HI(NT423), WI(NT424))$ arranged in E10.3 fields, six numbers per card. If i is in [1, NT421], j is in [1, NT422], k is in [1, NT423], and m is in [1, NT424] then the stress that corresponds to $VII(i), NZI(j), PI(k), WI(m)$ is the $((m-1) \cdot NT421 \cdot NT422 \cdot NT423 + (k-1) \cdot NT421 \cdot NT422 + (j-1) \cdot NT421 + i)$ th entry on these cards. The number $NT421 \cdot NT422 \cdot NT423 + NT424 \cdot NT421 \cdot NT422 \cdot NT423 \cdot NT424$ must not exceed 2000.

6 SAMPLE PROBLEM

A sample run is presented for the purpose of acquainting the user with the input data cards and the output. The data used does not represent any particular aircraft or usage. It is assumed that two control points are sufficient in this case to define the full scale aircraft fatigue spectrum. The input cards are as follows:

```

100  5  0  0  0  2  1  3  30 1973  23  12  2  21
   2  2  2  2  0  0  1
CHECK OUT RUN FOR SPECA PROGRAM
V G H DATA IN TABLE CONTROL POINT NUMBER 1 (REVISION 2)
   1  6  1
650.0  7.0  40000.0  36000.0  1.0  500.0
 101 123  1
20000.0 22000.0 24000.0 26000.0 28000.0 30000.0
32000.0 34000.0 36000.0 38000.0 40000.0 42000.0
44000.0 46000.0 48000.0 50000.0 52000.0 54000.0
56000.0 58000.0 60000.0 62000.0 64000.0
 201 212  1
0.05  0.10  0.20  0.25  0.30  0.40
0.50  0.60  0.70  0.80  0.90  0.95
 301 302  1
20000.0 35000.0

```


| 3.0 | 6.0 | 8.0 | | | |
|---------|---------|---------|---------|---------|---------|
| 5000.0 | 20000.0 | 35000.0 | | | |
| 25000.0 | 30000.0 | 35000.0 | | | |
| 10000.0 | 20000.0 | 24000.0 | 36000.0 | 39000.0 | 40000.0 |
| 45000.0 | 50000.0 | 53000.0 | 17000.0 | 18000.0 | 20000.0 |
| 25000.0 | 27000.0 | 30000.0 | 51000.0 | 53000.0 | 54000.0 |
| 15000.0 | 17000.0 | 18000.0 | 26000.0 | 28000.0 | 29000.0 |
| 32000.0 | 34000.0 | 36000.0 | 25000.0 | 26000.0 | 27000.0 |
| 42000.0 | 43000.0 | 44000.0 | 55000.0 | 56000.0 | 57000.0 |
| 21000.0 | 22000.0 | 24000.0 | 36000.0 | 38000.0 | 39000.0 |
| 55000.0 | 57000.0 | 58000.0 | 19000.0 | 21000.0 | 22000.0 |
| 30000.0 | 32000.0 | 33000.0 | 45000.0 | 46000.0 | 48000.0 |
| 27000.0 | 29000.0 | 32000.0 | 49000.0 | 50000.0 | 53000.0 |
| 62000.0 | 64000.0 | 65000.0 | 24000.0 | 25000.0 | 27000.0 |
| 39000.0 | 41000.0 | 42000.0 | 58000.0 | 60000.0 | 61000.0 |
| 22000.0 | 24000.0 | 25000.0 | 33000.0 | 35000.0 | 36000.0 |
| 48000.0 | 49000.0 | 51000.0 | | | |

Based on this input the following output listing was obtained.

RUN NO 100 DATE 8/30/1973 PAGE NO 1

CHECK OUT RUN FOR SPECIA PROGRAM
V C M DATA IN TABLE CONTROL POINT NUMBER 1 (REVISION 2)

HISTOGRAM SUBDIVISIONS

MMT = 2
MMZ = 2
MMW = 2
MMV = 2

LOAD MAGNIFICATION FACTOR = 1.0000

| INTERNAL LOAD LEVELS FOR INTEGRATION OF JOINT DENSITY FUNCTION | | | |
|--|------------|-----|------------|
| 1 | 2.0000E+04 | 2 | 2.2000E+04 |
| 2 | 2.5000E+04 | 6 | 3.0000E+04 |
| 3 | 3.0000E+04 | 10 | 3.5000E+04 |
| 4 | 3.5000E+04 | 14 | 4.0000E+04 |
| 5 | 4.0000E+04 | 18 | 4.5000E+04 |
| 6 | 4.5000E+04 | 22 | 5.0000E+04 |
| 7 | 5.0000E+04 | 26 | 5.5000E+04 |
| 8 | 5.5000E+04 | 30 | 6.0000E+04 |
| 9 | 6.0000E+04 | 34 | 6.5000E+04 |
| 10 | 6.5000E+04 | 38 | 7.0000E+04 |
| 11 | 7.0000E+04 | 42 | 7.5000E+04 |
| 12 | 7.5000E+04 | 46 | 8.0000E+04 |
| 13 | 8.0000E+04 | 50 | 8.5000E+04 |
| 14 | 8.5000E+04 | 54 | 9.0000E+04 |
| 15 | 9.0000E+04 | 58 | 9.5000E+04 |
| 16 | 9.5000E+04 | 62 | 1.0000E+05 |
| 17 | 1.0000E+05 | 66 | 1.0500E+05 |
| 18 | 1.0500E+05 | 70 | 1.1000E+05 |
| 19 | 1.1000E+05 | 74 | 1.1500E+05 |
| 20 | 1.1500E+05 | 78 | 1.2000E+05 |
| 21 | 1.2000E+05 | 82 | 1.2500E+05 |
| 22 | 1.2500E+05 | 86 | 1.3000E+05 |
| 23 | 1.3000E+05 | 90 | 1.3500E+05 |
| 24 | 1.3500E+05 | 94 | 1.4000E+05 |
| 25 | 1.4000E+05 | 98 | 1.4500E+05 |
| 26 | 1.4500E+05 | 102 | 1.5000E+05 |
| 27 | 1.5000E+05 | 106 | 1.5500E+05 |
| 28 | 1.5500E+05 | 110 | 1.6000E+05 |
| 29 | 1.6000E+05 | 114 | 1.6500E+05 |
| 30 | 1.6500E+05 | 118 | 1.7000E+05 |
| 31 | 1.7000E+05 | 122 | 1.7500E+05 |
| 32 | 1.7500E+05 | 126 | 1.8000E+05 |
| 33 | 1.8000E+05 | 130 | 1.8500E+05 |
| 34 | 1.8500E+05 | 134 | 1.9000E+05 |
| 35 | 1.9000E+05 | 138 | 1.9500E+05 |
| 36 | 1.9500E+05 | 142 | 2.0000E+05 |
| 37 | 2.0000E+05 | 146 | 2.0500E+05 |
| 38 | 2.0500E+05 | 150 | 2.1000E+05 |
| 39 | 2.1000E+05 | 154 | 2.1500E+05 |
| 40 | 2.1500E+05 | 158 | 2.2000E+05 |
| 41 | 2.2000E+05 | 162 | 2.2500E+05 |
| 42 | 2.2500E+05 | 166 | 2.3000E+05 |
| 43 | 2.3000E+05 | 170 | 2.3500E+05 |
| 44 | 2.3500E+05 | 174 | 2.4000E+05 |
| 45 | 2.4000E+05 | 178 | 2.4500E+05 |
| 46 | 2.4500E+05 | 182 | 2.5000E+05 |
| 47 | 2.5000E+05 | 186 | 2.5500E+05 |
| 48 | 2.5500E+05 | 190 | 2.6000E+05 |
| 49 | 2.6000E+05 | 194 | 2.6500E+05 |
| 50 | 2.6500E+05 | 198 | 2.7000E+05 |
| 51 | 2.7000E+05 | 202 | 2.7500E+05 |
| 52 | 2.7500E+05 | 206 | 2.8000E+05 |
| 53 | 2.8000E+05 | 210 | 2.8500E+05 |
| 54 | 2.8500E+05 | 214 | 2.9000E+05 |
| 55 | 2.9000E+05 | 218 | 2.9500E+05 |
| 56 | 2.9500E+05 | 222 | 3.0000E+05 |
| 57 | 3.0000E+05 | 226 | 3.0500E+05 |
| 58 | 3.0500E+05 | 230 | 3.1000E+05 |
| 59 | 3.1000E+05 | 234 | 3.1500E+05 |
| 60 | 3.1500E+05 | 238 | 3.2000E+05 |
| 61 | 3.2000E+05 | 242 | 3.2500E+05 |
| 62 | 3.2500E+05 | 246 | 3.3000E+05 |
| 63 | 3.3000E+05 | 250 | 3.3500E+05 |
| 64 | 3.3500E+05 | 254 | 3.4000E+05 |
| 65 | 3.4000E+05 | 258 | 3.4500E+05 |
| 66 | 3.4500E+05 | 262 | 3.5000E+05 |
| 67 | 3.5000E+05 | 266 | 3.5500E+05 |
| 68 | 3.5500E+05 | 270 | 3.6000E+05 |
| 69 | 3.6000E+05 | 274 | 3.6500E+05 |
| 70 | 3.6500E+05 | 278 | 3.7000E+05 |
| 71 | 3.7000E+05 | 282 | 3.7500E+05 |
| 72 | 3.7500E+05 | 286 | 3.8000E+05 |
| 73 | 3.8000E+05 | 290 | 3.8500E+05 |
| 74 | 3.8500E+05 | 294 | 3.9000E+05 |
| 75 | 3.9000E+05 | 298 | 3.9500E+05 |
| 76 | 3.9500E+05 | 302 | 4.0000E+05 |
| 77 | 4.0000E+05 | 306 | 4.0500E+05 |
| 78 | 4.0500E+05 | 310 | 4.1000E+05 |
| 79 | 4.1000E+05 | 314 | 4.1500E+05 |
| 80 | 4.1500E+05 | 318 | 4.2000E+05 |
| 81 | 4.2000E+05 | 322 | 4.2500E+05 |
| 82 | 4.2500E+05 | 326 | 4.3000E+05 |
| 83 | 4.3000E+05 | 330 | 4.3500E+05 |
| 84 | 4.3500E+05 | 334 | 4.4000E+05 |
| 85 | 4.4000E+05 | 338 | 4.4500E+05 |
| 86 | 4.4500E+05 | 342 | 4.5000E+05 |
| 87 | 4.5000E+05 | 346 | 4.5500E+05 |
| 88 | 4.5500E+05 | 350 | 4.6000E+05 |
| 89 | 4.6000E+05 | 354 | 4.6500E+05 |
| 90 | 4.6500E+05 | 358 | 4.7000E+05 |
| 91 | 4.7000E+05 | 362 | 4.7500E+05 |
| 92 | 4.7500E+05 | 366 | 4.8000E+05 |
| 93 | 4.8000E+05 | 370 | 4.8500E+05 |
| 94 | 4.8500E+05 | 374 | 4.9000E+05 |
| 95 | 4.9000E+05 | 378 | 4.9500E+05 |
| 96 | 4.9500E+05 | 382 | 5.0000E+05 |
| 97 | 5.0000E+05 | 386 | 5.0500E+05 |
| 98 | 5.0500E+05 | 390 | 5.1000E+05 |
| 99 | 5.1000E+05 | 394 | 5.1500E+05 |
| 100 | 5.1500E+05 | 398 | 5.2000E+05 |

CUMULATIVE AREAS OF LOAD PROBABILITY DENSITY FUNCTION

FOR SPECTRUM LOAD LEVELS

| | | | | | | | |
|---|------------|----|------------|----|------------|----|------------|
| 1 | 2.0000E-01 | 2 | 1.0000E-01 | 3 | 2.0000E-01 | 4 | 2.5000E-01 |
| 5 | 3.0000E-01 | 6 | 4.0000E-01 | 7 | 5.0000E-01 | 8 | 6.0000E-01 |
| 9 | 6.0000E-01 | 10 | 8.0000E-01 | 11 | 9.0000E-01 | 12 | 9.5000E-01 |

QUADRUPE TABLE NO. 1

PST VS VI, N7, M, W

VI

300.0 N7 500.0 600.0

3.0000 M 6.0000 8.0000

4000. M 20000. 35000.

25000. PST 30000. 35000.

20000. 21000. 25000.

30000. 31000. 35000.

40000. 41000. 45000.

50000. 51000. 55000.

60000. 61000. 65000.

70000. 71000. 75000.

80000. 81000. 85000.

90000. 91000. 95000.

100000. 101000. 105000.

110000. 111000. 115000.

120000. 121000. 125000.

130000. 131000. 135000.

140000. 141000. 145000.

150000. 151000. 155000.

160000. 161000. 165000.

170000. 171000. 175000.

180000. 181000. 185000.

190000. 191000. 195000.

200000. 201000. 205000.

210000. 211000. 215000.

220000. 221000. 225000.

230000. 231000. 235000.

240000. 241000. 245000.

250000. 251000. 255000.

260000. 261000. 265000.

270000. 271000. 275000.

280000. 281000. 285000.

290000. 291000. 295000.

300000. 301000. 305000.

310000. 311000. 315000.

320000. 321000. 325000.

330000. 331000. 335000.

340000. 341000. 345000.

350000. 351000. 355000.

360000. 361000. 365000.

370000. 371000. 375000.

380000. 381000. 385000.

390000. 391000. 395000.

400000. 401000. 405000.

410000. 411000. 415000.

420000. 421000. 425000.

430000. 431000. 435000.

440000. 441000. 445000.

450000. 451000. 455000.

460000. 461000. 465000.

470000. 471000. 475000.

480000. 481000. 485000.

490000. 491000. 495000.

500000. 501000. 505000.

510000. 511000. 515000.

520000. 521000. 525000.

530000. 531000. 535000.

| PUM NO | 100 | DATE | 6/30/1973 | PAGE NO | 4 |
|---|--------------|--------------|--------------|--------------|---------------|
| INTERNAL LOAD CUMULATIVE PROBABILITY FUNCTION | | | | | |
| INTERNAL LOAD | CUM PROB | LOAD | CUM PROB | LOAD | CUM PROB |
| 2.600000E+04 | 1.000000E+00 | 2.200000E+04 | 1.000000E+00 | 2.400000E+04 | 1.000000E+00 |
| 2.600000E+04 | 9.410190E-01 | 2.800000E+04 | 9.306560E-01 | 3.000000E+04 | 8.310203E-01 |
| 3.200000E+04 | 5.810719E-01 | 3.400000E+04 | 5.440577E-01 | 3.600000E+04 | 4.227598E-01 |
| 3.800000E+04 | 3.221785E-01 | 4.000000E+04 | 2.443382E-01 | 4.200000E+04 | 1.738435E-01 |
| 4.400000E+04 | 1.141107E-01 | 4.600000E+04 | 7.876584E-02 | 4.800000E+04 | 3.4801130E-02 |
| 5.000000E+04 | 1.780409E-02 | 5.200000E+04 | 1.443871E-03 | 5.400000E+04 | 1.447717E-04 |
| 5.600000E+04 | 0. | 5.800000E+04 | 0. | 6.000000E+04 | 0. |
| 6.200000E+04 | 0. | 6.400000E+04 | 0. | 0. | 0. |

| RUN NO | 100 | DATE | 8/30/1973 | PAGE NO | 5 |
|---|--------------|--------------|--------------|--------------|--------------|
| CUMULATIVE NUMBER OF EXCEEDANCES PER 1000 HRS | | | | | |
| LOAD | | LOAD | | LOAD | |
| 2.000000E+04 | 3.457400E+05 | 2.200000E+04 | 3.457400E+05 | 2.400000E+04 | 3.457400E+05 |
| 2.600000E+04 | 3.391775E+05 | 2.800000E+04 | 3.217650E+05 | 3.000000E+04 | 2.879795E+05 |
| 3.200000E+04 | 2.373025E+05 | 3.400000E+04 | 1.091025E+05 | 3.600000E+04 | 1.461650E+05 |
| 3.800000E+04 | 1.113900E+05 | 4.000000E+04 | 8.447950E+04 | 4.200000E+04 | 6.011075E+04 |
| 4.400000E+04 | 4.094250E+04 | 4.600000E+04 | 2.723250E+04 | 4.800000E+04 | 1.344950E+04 |
| 5.000000E+04 | 6.162500E+03 | 5.200000E+04 | 6.375000E+02 | 5.400000E+04 | 6.259900E+01 |
| 5.600000E+04 | 0. | 5.800000E+04 | 0. | 6.000000E+04 | 0. |
| 6.200000E+04 | 0. | 6.400000E+04 | 0. | 6.600000E+04 | 0. |

BASED ON 500.00 HOURS

| RUN NO | 100 | DATE | 02/10/1973 | PAGE NO | 6 |
|--|--------------|--------------|--------------|--------------|--------------|
| INTERNAL LOAD PROBABILITY DENSITY FUNCTION | | | | | |
| LOAD | PROB DEN | LOAD | PROB DEN | LOAD | PROB DEN |
| 2.000000E+04 | 3.957124E-14 | 2.200000E+04 | 7.562652E-19 | 2.400000E+04 | 4.745257E-06 |
| 2.600000E+04 | 1.713400E-05 | 2.800000E+04 | 3.716743E-05 | 3.000000E+04 | 6.116602E-05 |
| 3.200000E+04 | 7.180790E-05 | 3.400000E+04 | 6.562801E-05 | 3.600000E+04 | 5.546979E-05 |
| 3.800000E+04 | 6.60541E-05 | 4.000000E+04 | 3.707354E-05 | 4.200000E+04 | 3.155140E-05 |
| 4.400000E+04 | 2.37231E-05 | 4.600000E+04 | 1.974184E-05 | 4.800000E+04 | 1.523544E-05 |
| 5.000000E+04 | 9.780857E-06 | 5.200000E+04 | 4.418429E-06 | 5.400000E+04 | 4.605679E-07 |
| 5.600000E+04 | 6.714207E-06 | 5.800000E+04 | 0. | 6.000000E+04 | 0. |
| 6.200000E+04 | 0. | 6.400000E+04 | 0. | 0. | 0. |

| RUN NO | 100 | DATE | 8/30/1973 | PAGE NO | 7 |
|-----------------------------|-------------|----------|-------------|-------------|-------------|
| CYCLIC LOADING FRACTIONS | | | | | |
| | LOAD | FRACTION | LOAD | FRACTION | FRACTION |
| 2.76794E+04 | 7.50000E-02 | | 2.67279E+04 | 7.50000E-02 | 3.84308E+04 |
| 3.11175E+04 | 5.00000E-02 | | 3.14065E+04 | 7.50000E-02 | 3.31768E+04 |
| 1.46790E+04 | 1.00000E-01 | | 3.64153E+04 | 1.00000E-01 | 3.85501E+04 |
| 6.12075E+04 | 1.00000E-01 | | 4.49236E+04 | 7.50000E-02 | 4.73436E+04 |
| TOTAL LOAD CYCL S = 172870. | | | | | |

RUN NO 100 DATE 8/18/1978 PAGE NO 8
 CHECK OUT FOR SPECIA PROGRAM
 V G M DATA IN TA'LE CONTROL POINT NUMBER 2
 HISTOGRAM SURVIVALS
 NOUT = 2
 NONJ = 2
 NONI = 2
 NON = 2

LOAD MAGNIFICATION FACTOR = 1.0000

INTERNAL LOAD LEVELS FOR INTEGRATION OF JOINT DENSITY FUNCTION

| | | | | | | | |
|----|-------------|----|-------------|----|-------------|----|-------------|
| 1 | 2.00000E+04 | 2 | 2.20000E+04 | 3 | 2.40000E+04 | 4 | 2.60000E+04 |
| 5 | 2.80000E+04 | 6 | 3.00000E+04 | 7 | 3.20000E+04 | 8 | 3.40000E+04 |
| 9 | 3.60000E+04 | 10 | 3.80000E+04 | 11 | 4.00000E+04 | 12 | 4.20000E+04 |
| 13 | 4.40000E+04 | 14 | 4.60000E+04 | 15 | 4.80000E+04 | 16 | 5.00000E+04 |
| 17 | 5.20000E+04 | 18 | 5.40000E+04 | 19 | 5.60000E+04 | 20 | 5.80000E+04 |
| 21 | 6.00000E+04 | 22 | 6.20000E+04 | 23 | 6.40000E+04 | 24 | 6.60000E+04 |

CUMULATIVE AREAS OF LOAD PROBABILITY DENSITY FUNCTION FOR SURVIVOR LOAD LEVELS

| | | | | | | | |
|---|-------------|----|-------------|----|-------------|----|-------------|
| 1 | 5.00000E-01 | 2 | 1.00000E-01 | 3 | 2.00000E-01 | 4 | 2.50000E-01 |
| 5 | 3.00000E-01 | 6 | 4.00000E-01 | 7 | 5.00000E-01 | 8 | 6.00000E-01 |
| 9 | 7.00000E-01 | 10 | 8.00000E-01 | 11 | 9.00000E-01 | 12 | 9.50000E-01 |

PAGE NO 9

DATE 8/18/1973

SUN 100

BALANCED LOAD CONNECTION MATRIX

2.000000E+04 2.500000E+04
3.500000E+04 3.000000E+04

| PUN NO | 100 | DATE | 9/30/1973 | PAGE NO | 10 |
|-----------------------|-----|---------|-----------|---------|---------|
| QUADRUPLE TABLE NO. 1 | | | | | |
| PST VS VI, N7, M, & | | | | | |
| VI | | | | | |
| 300.0 | N7 | 500.0 | 600.0 | | |
| 3.0000 | M | 6.0000 | 8.0000 | | |
| 5000. | M | 20000. | 35000. | | |
| 25000. | M | 100000. | 35000. | | |
| PST | | | | | |
| 13000. | | 20000. | 24000. | 36000. | 39000. |
| 25000. | | 27000. | 30000. | 51000. | 53000. |
| 30000. | | 34000. | 36000. | 25000. | 26000. |
| 31000. | | 35000. | 36000. | 38000. | 39000. |
| 32000. | | 36000. | 37000. | 45000. | 46000. |
| 33000. | | 37000. | 38000. | 24000. | 25000. |
| 34000. | | 38000. | 39000. | 31000. | 35000. |
| 35000. | | 39000. | 40000. | 40000. | 45000. |
| 36000. | | 40000. | 41000. | 45000. | 50000. |
| 37000. | | 41000. | 42000. | 50000. | 55000. |
| 38000. | | 42000. | 43000. | 55000. | 60000. |
| 39000. | | 43000. | 44000. | 60000. | 65000. |
| 40000. | | 44000. | 45000. | 65000. | 70000. |
| 41000. | | 45000. | 46000. | 70000. | 75000. |
| 42000. | | 46000. | 47000. | 75000. | 80000. |
| 43000. | | 47000. | 48000. | 80000. | 85000. |
| 44000. | | 48000. | 49000. | 85000. | 90000. |
| 45000. | | 49000. | 50000. | 90000. | 95000. |
| 46000. | | 50000. | 51000. | 95000. | 100000. |
| 47000. | | 51000. | 52000. | 100000. | 105000. |
| 48000. | | 52000. | 53000. | 105000. | 110000. |
| 49000. | | 53000. | 54000. | 110000. | 115000. |
| 50000. | | 54000. | 55000. | 115000. | 120000. |
| 51000. | | 55000. | 56000. | 120000. | 125000. |
| 52000. | | 56000. | 57000. | 125000. | 130000. |
| 53000. | | 57000. | 58000. | 130000. | 135000. |
| 54000. | | 58000. | 59000. | 135000. | 140000. |
| 55000. | | 59000. | 60000. | 140000. | 145000. |
| 56000. | | 60000. | 61000. | 145000. | 150000. |
| 57000. | | 61000. | 62000. | 150000. | 155000. |
| 58000. | | 62000. | 63000. | 155000. | 160000. |
| 59000. | | 63000. | 64000. | 160000. | 165000. |
| 60000. | | 64000. | 65000. | 165000. | 170000. |
| 61000. | | 65000. | 66000. | 170000. | 175000. |
| 62000. | | 66000. | 67000. | 175000. | 180000. |
| 63000. | | 67000. | 68000. | 180000. | 185000. |
| 64000. | | 68000. | 69000. | 185000. | 190000. |
| 65000. | | 69000. | 70000. | 190000. | 195000. |
| 66000. | | 70000. | 71000. | 195000. | 200000. |
| 67000. | | 71000. | 72000. | 200000. | 205000. |
| 68000. | | 72000. | 73000. | 205000. | 210000. |
| 69000. | | 73000. | 74000. | 210000. | 215000. |
| 70000. | | 74000. | 75000. | 215000. | 220000. |
| 71000. | | 75000. | 76000. | 220000. | 225000. |
| 72000. | | 76000. | 77000. | 225000. | 230000. |
| 73000. | | 77000. | 78000. | 230000. | 235000. |
| 74000. | | 78000. | 79000. | 235000. | 240000. |
| 75000. | | 79000. | 80000. | 240000. | 245000. |
| 76000. | | 80000. | 81000. | 245000. | 250000. |
| 77000. | | 81000. | 82000. | 250000. | 255000. |
| 78000. | | 82000. | 83000. | 255000. | 260000. |
| 79000. | | 83000. | 84000. | 260000. | 265000. |
| 80000. | | 84000. | 85000. | 265000. | 270000. |
| 81000. | | 85000. | 86000. | 270000. | 275000. |
| 82000. | | 86000. | 87000. | 275000. | 280000. |
| 83000. | | 87000. | 88000. | 280000. | 285000. |
| 84000. | | 88000. | 89000. | 285000. | 290000. |
| 85000. | | 89000. | 90000. | 290000. | 295000. |
| 86000. | | 90000. | 91000. | 295000. | 300000. |
| 87000. | | 91000. | 92000. | 300000. | 305000. |
| 88000. | | 92000. | 93000. | 305000. | 310000. |
| 89000. | | 93000. | 94000. | 310000. | 315000. |
| 90000. | | 94000. | 95000. | 315000. | 320000. |
| 91000. | | 95000. | 96000. | 320000. | 325000. |
| 92000. | | 96000. | 97000. | 325000. | 330000. |
| 93000. | | 97000. | 98000. | 330000. | 335000. |
| 94000. | | 98000. | 99000. | 335000. | 340000. |
| 95000. | | 99000. | 100000. | 340000. | 345000. |

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| CUMULATIVE NUMBER OF EXCEEDANCES PER 1000 HRS | | | |
|---|--------------|-------------|--------------|
| LOAD | EXCEEDANCES | LOAD | EXCEEDANCES |
| 2.00000E+04 | 3.457400E+05 | 2.20000E+04 | 3.457400E+05 |
| 2.40000E+04 | 3.191775E+05 | 2.40000E+04 | 3.217650E+05 |
| 2.80000E+04 | 2.161775E+05 | 2.60000E+04 | 1.871650E+05 |
| 3.20000E+04 | 1.106525E+05 | 2.80000E+04 | 8.276500E+04 |
| 3.60000E+04 | 3.750375E+04 | 3.00000E+04 | 2.246125E+04 |
| 4.00000E+04 | 1.637500E+03 | 3.20000E+04 | 2.625000E+02 |
| 4.40000E+04 | 0. | 3.40000E+04 | 0. |
| 4.80000E+04 | 0. | 3.60000E+04 | 0. |
| 5.20000E+04 | 0. | 3.80000E+04 | 0. |
| 5.60000E+04 | 0. | 4.00000E+04 | 0. |
| 6.00000E+04 | 0. | 4.20000E+04 | 0. |
| 6.40000E+04 | 0. | 4.40000E+04 | 0. |
| 6.80000E+04 | 0. | 4.60000E+04 | 0. |
| 7.20000E+04 | 0. | 4.80000E+04 | 0. |
| 7.60000E+04 | 0. | 5.00000E+04 | 0. |
| 8.00000E+04 | 0. | 5.20000E+04 | 0. |
| 8.40000E+04 | 0. | 5.40000E+04 | 0. |
| 8.80000E+04 | 0. | 5.60000E+04 | 0. |
| 9.20000E+04 | 0. | 5.80000E+04 | 0. |
| 9.60000E+04 | 0. | 6.00000E+04 | 0. |
| 1.00000E+05 | 0. | 6.20000E+04 | 0. |
| 1.04000E+05 | 0. | 6.40000E+04 | 0. |
| 1.08000E+05 | 0. | 6.60000E+04 | 0. |
| 1.12000E+05 | 0. | 6.80000E+04 | 0. |
| 1.16000E+05 | 0. | 7.00000E+04 | 0. |
| 1.20000E+05 | 0. | 7.20000E+04 | 0. |
| 1.24000E+05 | 0. | 7.40000E+04 | 0. |
| 1.28000E+05 | 0. | 7.60000E+04 | 0. |
| 1.32000E+05 | 0. | 7.80000E+04 | 0. |
| 1.36000E+05 | 0. | 8.00000E+04 | 0. |
| 1.40000E+05 | 0. | 8.20000E+04 | 0. |
| 1.44000E+05 | 0. | 8.40000E+04 | 0. |
| 1.48000E+05 | 0. | 8.60000E+04 | 0. |
| 1.52000E+05 | 0. | 8.80000E+04 | 0. |
| 1.56000E+05 | 0. | 9.00000E+04 | 0. |
| 1.60000E+05 | 0. | 9.20000E+04 | 0. |
| 1.64000E+05 | 0. | 9.40000E+04 | 0. |
| 1.68000E+05 | 0. | 9.60000E+04 | 0. |
| 1.72000E+05 | 0. | 9.80000E+04 | 0. |
| 1.76000E+05 | 0. | 1.00000E+05 | 0. |

BASED ON 500.00 HOURS

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| INTERNAL LOAD PROBABILITY DENSITY FUNCTION | | | |
|--|-------------|-------------|-------------|
| LOAD | PROB DEN | LOAD | PROB DEN |
| 2.00000E+04 | 3.95732E-15 | 2.20000E+04 | 6.56265E-19 |
| 2.40000E+04 | 1.71160E-05 | 2.40000E+04 | 6.17425E-05 |
| 2.80000E+04 | 7.25558E-05 | 2.60000E+04 | 3.71076E-05 |
| 3.20000E+04 | 6.52207E-05 | 2.80000E+04 | 6.58460E-05 |
| 3.60000E+04 | 2.52979E-05 | 3.00000E+04 | 3.74714E-05 |
| 4.00000E+04 | 6.76718E-06 | 3.20000E+04 | 2.01614E-05 |
| 4.40000E+04 | 4.51929E-06 | 3.40000E+04 | 1.13862E-06 |
| 4.80000E+04 | 2.76718E-06 | 3.60000E+04 | 0. |
| 5.20000E+04 | 0. | 3.80000E+04 | 0. |
| 5.60000E+04 | 0. | 4.00000E+04 | 0. |
| 6.00000E+04 | 0. | 4.20000E+04 | 0. |
| 6.20000E+04 | 0. | 4.40000E+04 | 0. |
| 6.40000E+04 | 0. | 4.60000E+04 | 0. |
| 6.60000E+04 | 0. | 4.80000E+04 | 0. |
| 6.80000E+04 | 0. | 5.00000E+04 | 0. |
| 7.00000E+04 | 0. | 5.20000E+04 | 0. |
| 7.20000E+04 | 0. | 5.40000E+04 | 0. |
| 7.40000E+04 | 0. | 5.60000E+04 | 0. |
| 7.60000E+04 | 0. | 5.80000E+04 | 0. |
| 7.80000E+04 | 0. | 6.00000E+04 | 0. |
| 8.00000E+04 | 0. | 6.20000E+04 | 0. |
| 8.20000E+04 | 0. | 6.40000E+04 | 0. |
| 8.40000E+04 | 0. | 6.60000E+04 | 0. |
| 8.60000E+04 | 0. | 6.80000E+04 | 0. |
| 8.80000E+04 | 0. | 7.00000E+04 | 0. |
| 9.00000E+04 | 0. | 7.20000E+04 | 0. |
| 9.20000E+04 | 0. | 7.40000E+04 | 0. |
| 9.40000E+04 | 0. | 7.60000E+04 | 0. |
| 9.60000E+04 | 0. | 7.80000E+04 | 0. |
| 9.80000E+04 | 0. | 8.00000E+04 | 0. |
| 1.00000E+05 | 0. | 8.20000E+04 | 0. |
| 1.20000E+05 | 0. | 8.40000E+04 | 0. |
| 1.40000E+05 | 0. | 8.60000E+04 | 0. |
| 1.60000E+05 | 0. | 8.80000E+04 | 0. |
| 1.80000E+05 | 0. | 9.00000E+04 | 0. |
| 2.00000E+05 | 0. | 9.20000E+04 | 0. |
| 2.20000E+05 | 0. | 9.40000E+04 | 0. |
| 2.40000E+05 | 0. | 9.60000E+04 | 0. |
| 2.60000E+05 | 0. | 9.80000E+04 | 0. |
| 2.80000E+05 | 0. | 1.00000E+05 | 0. |
| 3.00000E+05 | 0. | | |
| 3.20000E+05 | 0. | | |
| 3.40000E+05 | 0. | | |
| 3.60000E+05 | 0. | | |
| 3.80000E+05 | 0. | | |
| 4.00000E+05 | 0. | | |
| 4.20000E+05 | 0. | | |
| 4.40000E+05 | 0. | | |
| 4.60000E+05 | 0. | | |
| 4.80000E+05 | 0. | | |
| 5.00000E+05 | 0. | | |
| 5.20000E+05 | 0. | | |
| 5.40000E+05 | 0. | | |
| 5.60000E+05 | 0. | | |
| 5.80000E+05 | 0. | | |
| 6.00000E+05 | 0. | | |
| 6.20000E+05 | 0. | | |
| 6.40000E+05 | 0. | | |
| 6.60000E+05 | 0. | | |
| 6.80000E+05 | 0. | | |
| 7.00000E+05 | 0. | | |
| 7.20000E+05 | 0. | | |
| 7.40000E+05 | 0. | | |
| 7.60000E+05 | 0. | | |
| 7.80000E+05 | 0. | | |
| 8.00000E+05 | 0. | | |
| 8.20000E+05 | 0. | | |
| 8.40000E+05 | 0. | | |
| 8.60000E+05 | 0. | | |
| 8.80000E+05 | 0. | | |
| 9.00000E+05 | 0. | | |
| 9.20000E+05 | 0. | | |
| 9.40000E+05 | 0. | | |
| 9.60000E+05 | 0. | | |
| 9.80000E+05 | 0. | | |
| 1.00000E+06 | 0. | | |

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 CYCLIC LOADING FRACTIONS
 LOAD FRACTION LOAD FRACTION LOAD FRACTION
 2.72095E+04 7.50000E-02 2.87315E+04 7.50000E-02 3.02195E+04 7.50000E-02
 3.10011E+04 5.70000E-01 3.17753E+04 7.50000E-02 3.31391E+04 1.00000E-01
 3.45504E+04 1.70000E-01 3.61720E+04 1.00000E-01 3.74758E+04 1.00000E-01
 3.80655E+04 1.00000E-01 4.03457E+04 7.50000E-02 4.27184E+04 7.50000E-02
 TOTAL LOAD CYCLES = 172870

001 ON FILE

| | | | |
|----|--------------------------------------|----|--------------------------------------|
| 1 | COEFFICIENTS FOR FREQUENCY LEVEL NO. | 1 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 2 | -2.693999E+00 -1.006776E+00 | 7 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 3 | COEFFICIENTS FOR FREQUENCY LEVEL NO. | 8 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 4 | -2.611910E+00 -2.049164E+00 | 9 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 5 | COEFFICIENTS FOR FREQUENCY LEVEL NO. | 10 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 6 | -2.756611E+00 -2.112331E+00 | 11 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 7 | COEFFICIENTS FOR FREQUENCY LEVEL NO. | 12 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 8 | -2.820644E+00 -2.261333E+00 | 13 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 9 | COEFFICIENTS FOR FREQUENCY LEVEL NO. | 14 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 10 | -2.898464E+00 -2.318007E+00 | 15 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 11 | COEFFICIENTS FOR FREQUENCY LEVEL NO. | 16 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 12 | -3.011644E+00 -2.410121E+00 | 17 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 13 | COEFFICIENTS FOR FREQUENCY LEVEL NO. | 18 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 14 | -2.169619E+00 -2.119416E+00 | 19 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 15 | COEFFICIENTS FOR FREQUENCY LEVEL NO. | 20 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 16 | -3.306817E+00 -2.646643E+00 | 21 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 17 | COEFFICIENTS FOR FREQUENCY LEVEL NO. | 22 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 18 | -2.540740E+00 -2.708767E+00 | 23 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 19 | COEFFICIENTS FOR FREQUENCY LEVEL NO. | 24 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 20 | -2.733233E+00 -2.086745E+00 | 25 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 21 | COEFFICIENTS FOR FREQUENCY LEVEL NO. | 26 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 22 | -2.033414E+00 -3.257621E+00 | 27 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 23 | COEFFICIENTS FOR FREQUENCY LEVEL NO. | 28 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 24 | -2.242171E+00 -3.197737E+00 | 29 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |
| 25 | COEFFICIENTS FOR FREQUENCY LEVEL NO. | 30 | COEFFICIENTS FOR FREQUENCY LEVEL NO. |

```
CAT-OF-FILE ENCODED. FILENAME = INPUT  
EASOR NUMBER   COPS DETECTED BY INDC= AT ADDRESS 000160  
CALLED FROM    INPUT AT LINE 0161  
CALLED FROM    CUTCP AT LINE 017  
CALLED FROM    SPSCA AT LINE 019
```


SECTION IV

EXAMPLE PROBLEM - F-4 STRESS SPECTRUM FOR POSITIVE LOAD FACTORS

The data base for this problem is four quarters of VGH data starting with the second quarter of 1972 and finishing with the first quarter of 1973. The VGH histogram intervals for these data are the following:

Indicated airspeed (knots)

150, 200, 250, 300, 350, 400, 450, 500, 550, 625, and 700

Normal load factor (equivalent)

1.4, 1.8, 2.2, 2.6, 3.0, 3.8, 4.6, 5.4, 6.6, 7.8, and 9.0

Altitude (feet)

0, 1000, 2000, 5000, 10,000, 15,000, 20,000, 30,000, 40,000, and 50,000

Weight (pounds)

37,500 (reference weight)

The stress table was set up with the following indicated airspeed, normal load factor, altitude, and weight combinations:

Indicated airspeed (knots)

175, 225, 275, 325, 375, 425, 475, 525, 575, and 625

Normal load factor

2.4, 2.8, 3.4, 4.2, 5.0, 6.0, 7.2, and 8.9

Altitude (feet)

500, 1500, 3500, 7500, 12500, 17500, 25000, and 35000

Weight (pounds)

37,500

The VGH histogram table was made up using all of the available data for the air-to-air and air-to-ground operations for the four quarters without distinguishing the various F-4 models except that only the unslatted configurations were considered. The numbers of hours of data in each category and their corresponding numbers of positive and negative load occurrences are shown in Table 1.

The number of stress exceedances per 1000 hours for load reference station (LRS) 180, defined in Figure 1 is shown in Figure 2 through Figure 7. Figure 2 through Figure 5 shows the variation from quarter to quarter of the VGH data. The stress exceedance graphs appear to show a small degree of scatter except for the SEA air-to-air first quarter where there was an overt change in the mission although it was still categorized as air-to-air. The four quarters of data are combined in Figures 6 and 7 to show the differences between the CONUS and SEA in the air-to-air operation and the air-to-ground operation.

SECTION V

CONCLUSIONS

The procedure described in this report can eliminate much of the uncertainty that can occur in the derivation of the maneuver load stress spectrum. For new aircraft an estimate must be made of the VGH histogram to obtain the spectrum. This estimate can be updated during Task V of ASIP to derive a better estimate for the operational life of the fleet. This procedure can be immediately applied to fleet tracking by computing the conditional probability of exceeding a stress level given the normal load factor.

The application to full scale aircraft testing makes use of the assumption that the stress is matched at a specified number of control points by a linear combination of the same number of balanced loading conditions. This technique is believed to be more accurate than the usual process of a damage match at the specified control points in that the troublesome damage calculation is eliminated. The stress spectra at points other than control points are presumed to be matched satisfactorily by using representative loading conditions. It is, of course, theoretically better to use all points of the sky that occur in the VGH histogram. This, however, may be impractical due to test equipment limitations.

The procedure as applied to the F-4 fleet indicates that in general the stress spectra do not show significant changes from quarter to quarter. Also, when an operational change is made the method will reflect that change. When CONUS and SEA data are compared there appears to be a reasonably good correlation between the spectra generated in training and the spectra generated in combat.

TABLE 1. F-4 VGH DATA SUMMARY

| PERIOD | TYPE | HOURS | + COUNTS | - COUNTS | TOTAL COUNTS |
|--------|----------|---------|----------|----------|--------------|
| 2Q 72 | CONUS AA | 196.87 | 13981 | 4541 | 18522 |
| 2Q 72 | SEA AA | 65.84 | 4047 | 662 | 4709 |
| 2Q 72 | CONUS AG | 251.70 | 30723 | 9432 | 40155 |
| 2Q 72 | SEA AG | 1248.94 | 93027 | 13258 | 106285 |
| 3Q 72 | CONUS AA | 290.22 | 17470 | 5259 | 22729 |
| 3Q 72 | SEA AA | 393.26 | 30842 | 6366 | 37208 |
| 3Q 72 | CONUS AG | 469.64 | 38968 | 9934 | 48902 |
| 3Q 72 | SEA AG | 802.74 | 66446 | 12485 | 78931 |
| 4Q 72 | CONUS AA | 184.92 | 9404 | 3138 | 12542 |
| 4Q 72 | SEA AA | 164.35 | 7862 | 1933 | 9795 |
| 4Q 72 | CONUS AG | 89.16 | 5959 | 1265 | 7224 |
| 4Q 72 | SEA AA | 502.09 | 28254 | 4819 | 33073 |
| 1Q 73 | CONUS AA | 123.18 | 7983 | 2231 | 10214 |
| 1Q 73 | SEA AA | 133.96 | 6100 | 1358 | 7458 |
| 1Q 73 | CONUS AG | 194.38 | 17828 | 4001 | 21829 |
| 1Q 73 | SEA AG | 933.87 | 42342 | 8229 | 50571 |

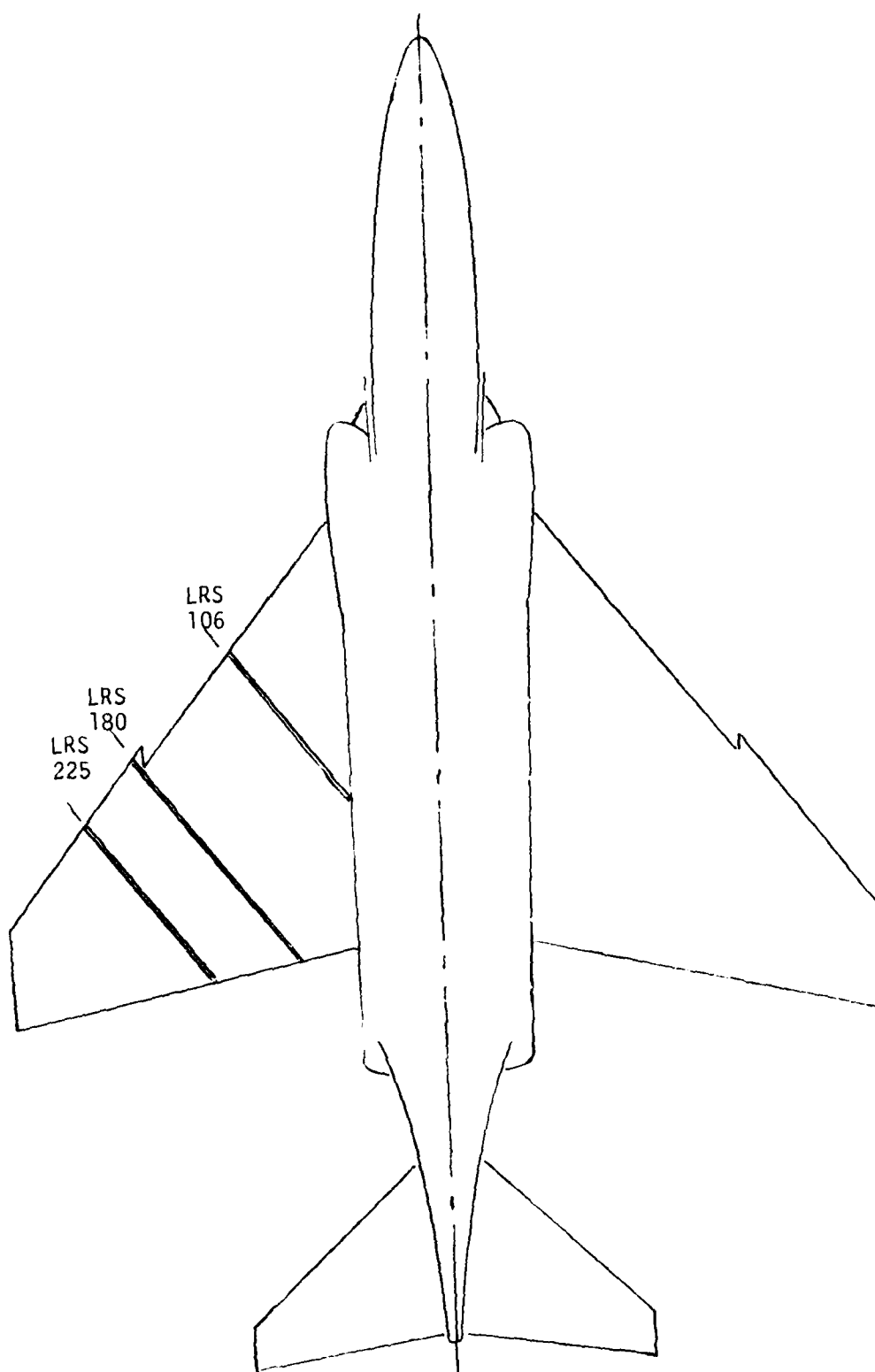


Figure 1. F-4 Wing Load Reference Station Locations

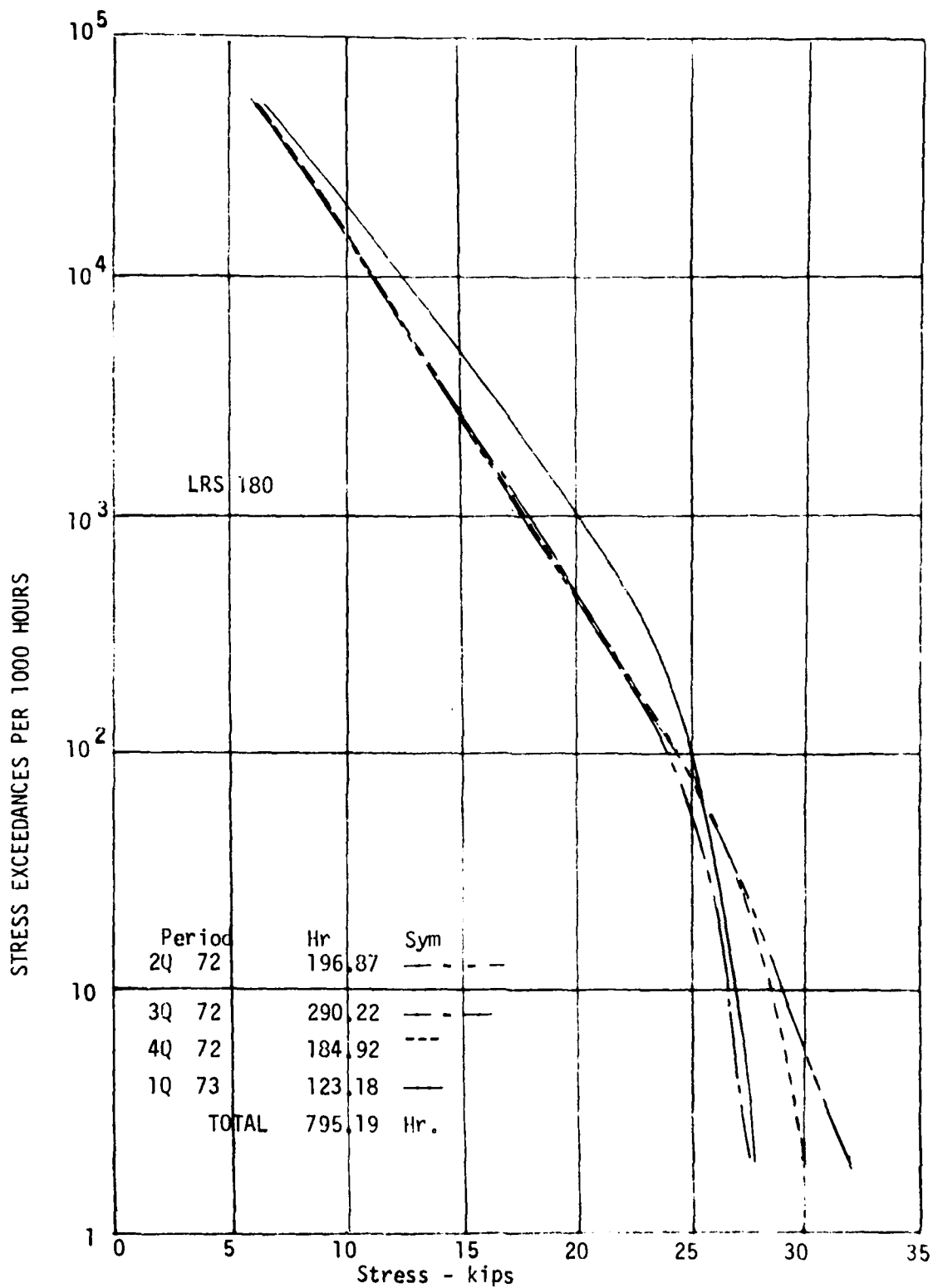


Figure 2. F-4 Spectra - CONUS Air-to-Air (All Models)

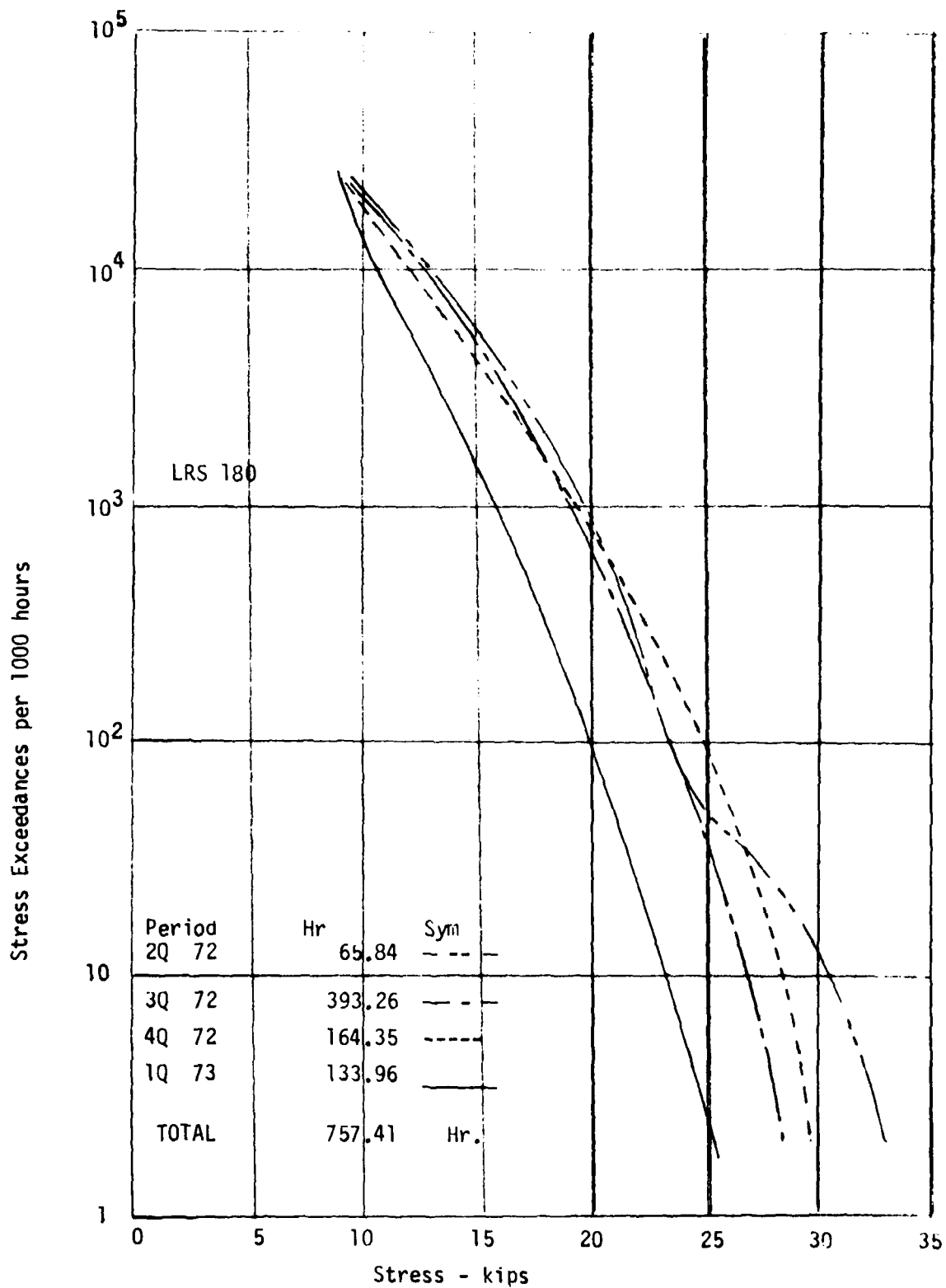


Figure 3. F-4 Spectra - SEA Air-to-Air (All Models)

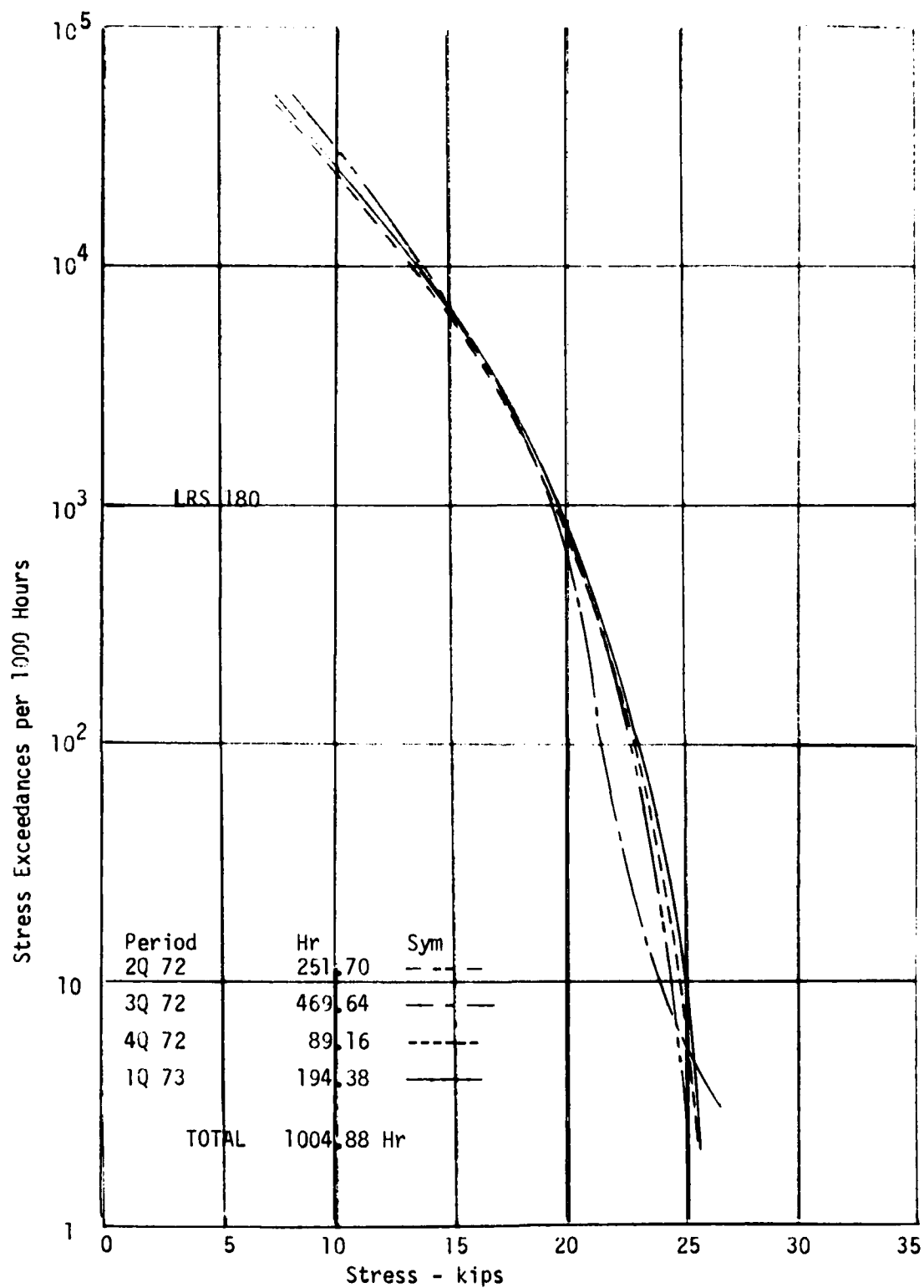


Figure 4. F-4 Spectra - CONUS Air-to-Ground (All Models)

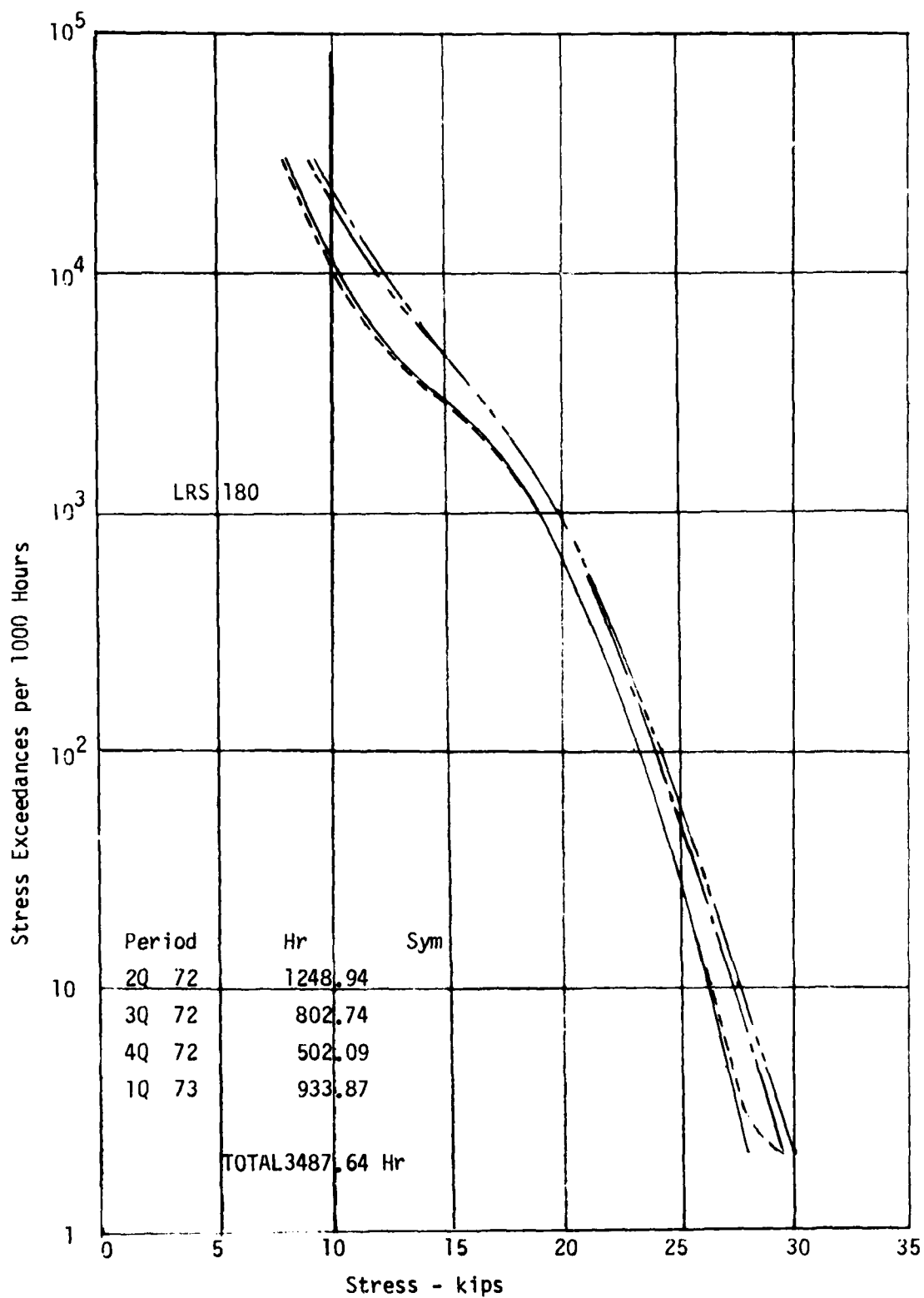


Figure 5. F-1 Spectra - SEA Air-to-Ground (All Models)

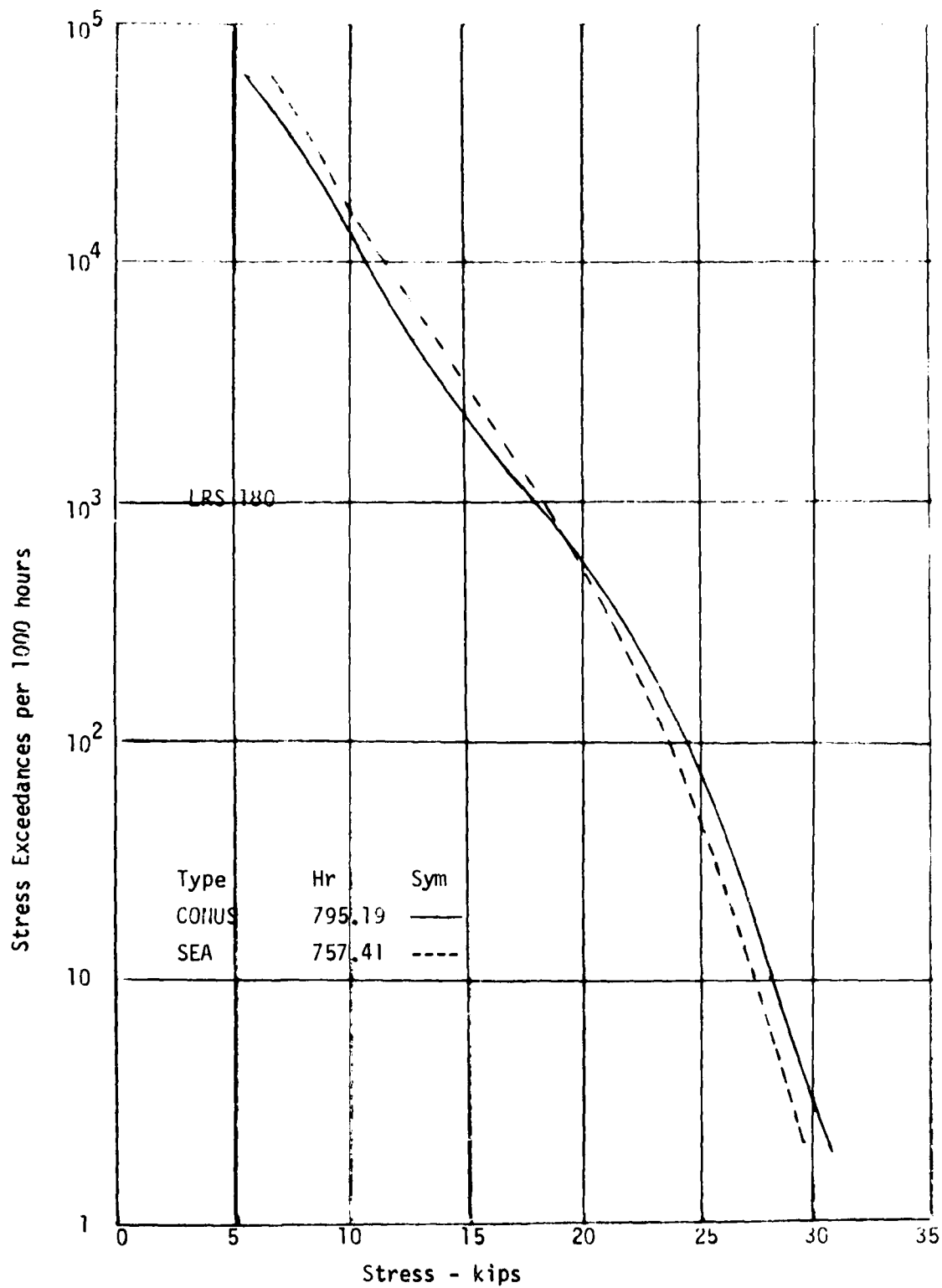


Figure 6. F-4 Spectra - Air-to-Air (All Models)
for One Year of VGH Data

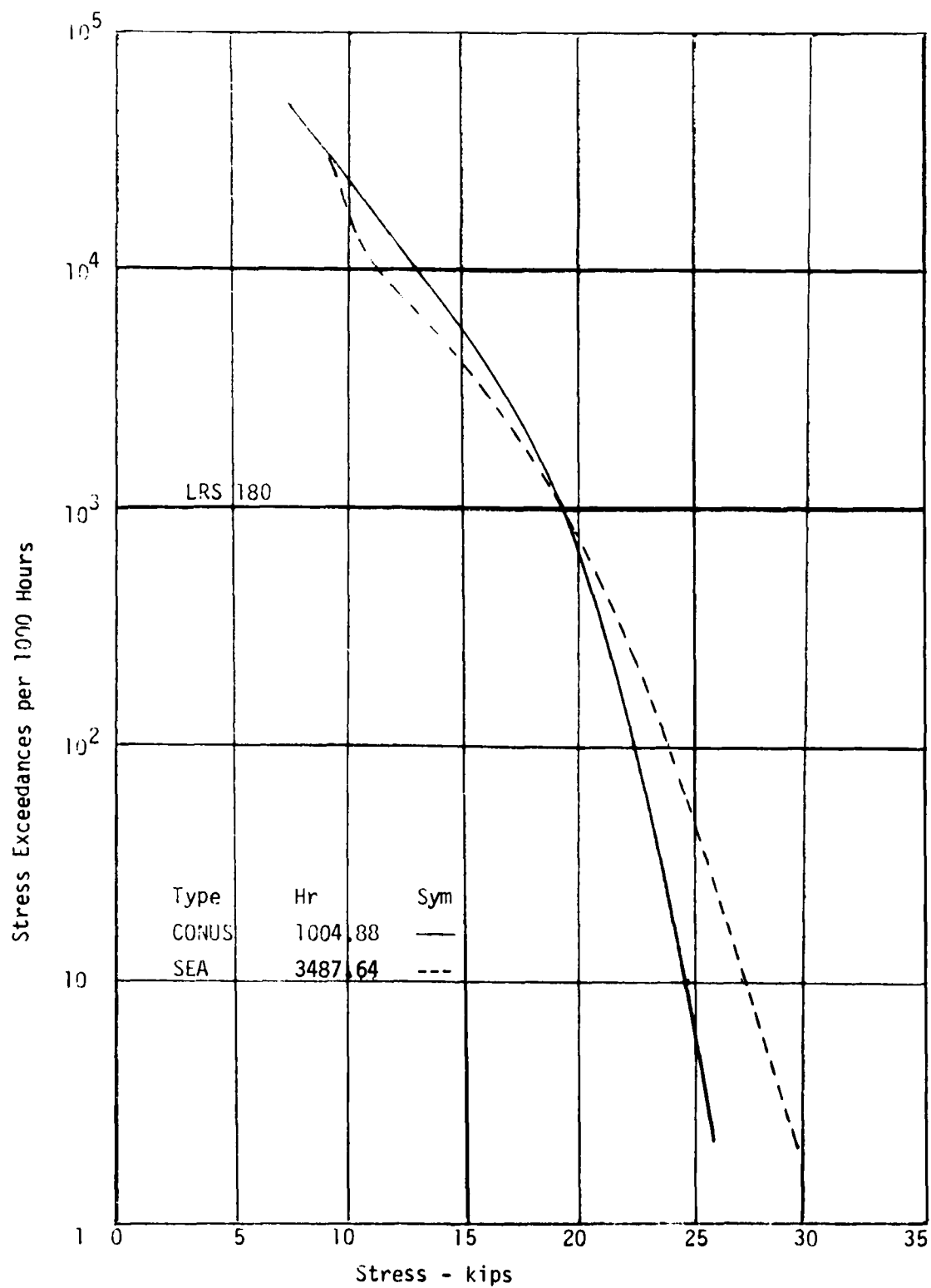


Figure 7. F-4 Spectra - Air-to-Ground (All Models)
for One Year of VGH Data

APPENDIX - SPECA PROGRAM LISTING

The listing given below is a FORTRAN extended language routine. This listing contains all of the statements for the version described in the Introduction of this report. Section 3.3 gives a brief description of each of the sub-routines in this listing.

```

PROGRAM SPECI INPUT, OUTPUT, TAPLS=INPUT, TAPEL=OUTPUT
PROGRAM FOR COMPUTING AIRCRAFT INTERNAL LOAD PROBABILITY
DENSITY FUNCTIONS
REVISION 2 COMMON P(10000), NTEGER(1000), TAPL(12000,2),
5      1 TAPL(1500,1)
      EQUIVALENCE (NTEGER(48), NZERO), (NTEGER(50), MPSCF)
      NZERO = 0
      MPSCF = 0
      CALL GUJDI
      GO TO 10
      ENJ
10
30

```

```

MAIN 1
MAIN 2
MAIN 21
MAIN 3
MAIN 31
MAIN 4
MAIN 5
MAIN 51
MAIN 6
MAIN 7
MAIN 8

```

| SUBROUTINE GUIDE | | SUBROUTINE GUIDE | |
|------------------|----|--|----------|
| C | | SUBROUTINE FOR CALLING INPUT DATA AND CALCULATING ROUTINES | GIDE |
| 5 | 1 | COMMON F(10000), INTEGER(100), TABL4(2000,2), | GIDE 2 |
| | | TABL2(500,1) | GIDE 3 |
| | | EQUIVALENCE (INTEGER(1), MPS) | GIDE 31 |
| | | EQUIVALENCE (INTEGER(40), NZERO) | GIDE 32 |
| | | IF (NZERO) 40, 10 | GIDE 4 |
| 10 | 20 | DO 20 I = 1, 10000 | GIDE 41 |
| | | P(I) = 0.0 | GIDE 5 |
| | | DO 30 I = 1, 100 | GIDE 6 |
| | | INTEGER(I) = 0 | GIDE 7 |
| | | GO TO 44 | GIDE 8 |
| 30 | 40 | DO 47 I = 1001, 10000 | GIDE 81 |
| | | P(I) = 0.0 | GIDE 9 |
| | | FACTOR = 1.0 | GIDE 91 |
| 15 | 42 | CALL INPUT | GIDE 92 |
| | | CALL CALC | GIDE 93 |
| | | CALL LDVVL | GIDE 10 |
| 20 | | CALL PRINTP | GIDE 11 |
| | | IF (MPS) 60, 60, 50 | GIDE 12 |
| | | CALL LOGOLF | GIDE 121 |
| | 50 | RETURN | GIDE 122 |
| | 60 | END | GIDE 13 |
| | | | GIDE 14 |

| SUBROUTINE INPUT | 7474 | OPT=1 | FINA-04P353 | 11/02/73 09:55:18 | PAGE 1 |
|------------------|-------------------|-------|---|-------------------|--|
| 115 | | | READ (5,140) (TABLK(K,I), K = 1, NNT13) READ (5,140) (TABLK(K,I), K = NNT13+1, NNT112) READ (5,140) (TABLK(K,I), K = NNT12+1, NNT113) GO TO (654,656), I GO TO (656,660), NTD | | DEIN1004 DEIN1005 DEIN1006 DEIN1007 DEIN1008 |
| 120 | 654 656 | | READ (5,140) (TABLK(K,I), K = NNT13+1, NNT114) READ (5,140) (TABLK(K,I), K = NNT14+1, NNT115) GO TO 670 | | DEIN1009 DEIN1010 DEIN1011 |
| 125 | 660 870 870 | | READ (5,140) NNT13 NF = NNT13 + NTP READ (5,140) (TABLK(K,I), K = NNT13+1, NF) CONTINUE CALL INALC RETURN END | | DEIN1012 DEIN1013 DEIN1014 DEIN1015 DEIN1016 DEIN1017 DEIN1018 DEIN1019 DEIN1020 DEIN1021 |


```

306  FORMAT (10E15.5)
39  IF (INT4) 150, 150, 40
40  DO 130 I = 1, 2
41  IF (INT4(I)) 50, 130
50  NT1 = NT4(I)
    NT2 = NT4(2)
    NT3 = NT4(3)
    NT4 = NT4(4)
    NTP = NT1 + NT2 + NT3 + NT4
    NT1P1 = NT1 + 1
    NT112 = NT1 + NT2
    NT12P1 = NT112 + 1
    NT113 = NT112 + NT3
    NT13P1 = NT113 + 1
    NT114 = NT113 + NT4
    NT14P1 = NT114 + 1
    NF = NT114 + NTP
    NT4 = NT114 + 1
    CALL PAGEAU
    GO TO 152, C21, I
52  WRITE (6, J)
56  FORMAT (10X, 21CUCUCUFILE TABLE NO. 1 / 10X,
    1  19HPSI VS VI, NZ, M, W)
    GO TO 72
62  NNT1 (6, 64)
64  FORMAT (10X, 21CUCUCUFILE TABLE NO. 2 / 10X,
    1  21HPSI VS VI, NZ, M, W)
66  WRITE (6, 70) (TABL4(J, I), J = 1, 5, NNT1)
70  FORMAT (10X, 2HVI / (12F9.1))
    GO TO 74
72  WRITE (6, 73) (TABL4(J, I), J = 1, NNT1)
74  FORMAT (10X, 2HVI / (12F9.1))
76  WRITE (6, 80) (TABL4(J, I), J = NNT1P1, NNT112)
80  FORMAT (10X, 2HVI / (12F9.1))
78  WRITE (6, 90) (TABL4(J, I), J = NNT1P1, NNT113)
90  FORMAT (10X, 1H / (12F9.1))
    GO TO 94, 96, I
94  WRITE (6, 96) (TABL4(J, I), J = NNT1P1, NNT114)
96  WRITE (6, 100) (TABL4(J, I), J = NNT1P1, NNT114)
    GO TO 101
98  WRITE (6, 100) NNT13
100  FORMAT (10X, 1H / (12F9.1))
    GO TO (102, 112), I
102  GO TO (104, 106), NTP
104  WRITE (6, 110) (TABL4(J, I), J = NNT1P1, NF)
    GO TO 130
106  NF = NNT113 + NTP
    WRITE (6, 110) (TABL4(J, I), J = NNT1P1, NF)
110  FORMAT (10X, 3HPSI / (12F10.0))
    GO TO 130
112  WRITE (6, 120) (TABL4(J, I), J = NNT1P1, NF)
120  FORMAT (10X, 5HPSI / (12F10.0))
130  CONTINUE
140  IF (INT4(12)) 150, 150, 142
142  WRITE (6, 140) FVI, FNZ, FM, FM
144  FORMAT (10X, 25HLAST ASCISSAS IN TABLE 2 /
    1  10X, 8HVI = , E15.6 /

```

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FTN A-000363

OPT=1

74274

SUBROUTINE INAD

114
104, 0MFM2 = E15.6 /
104, 0MFM = E15.6 /
104, 0MFM = E15.6 /
NZERO = 1
RETURN
END

INAD 67
INAD 68
INAD 69
INAD 80
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INAD 91

120

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115      WRITE (6,70) K3
120      FORMAT (10X, 20GAUSS2 EXPOR SIGNAL + K3 = , 13)
125      IF (I-1) 140, 100, 90
130      IF (I-MPLP2) 120, 110, 140
135      POPSI(1) = 2.0 * X(1) * PSIL(1) + X(2)
140      GO TO 120
145      POPSI(1) = 2.0 * X(1) * PSIL(1) + X(2)
150      POPSI(1) = 2.0 * X(1) * PSIL(1) + X(2)
155      CONTINUE
160      RETURN
165      END

```

CALC 22
 CALC 23
 CALC 24
 CALC 25
 CALC 26
 CALC 27
 CALC 28
 CALC 29
 CALC 30
 CALC 31
 CALC 32

```
      C SUBROUTINE FOR COMPUTING INTERNAL LOAD LEVELS FOR
      C A GIVEN DISTRIBUTION OF LOAD CYCLES
      C
      C COMMON P410000, NTEGER(100), FARL4(2000,2),
      C
      C DIMENSION PPSI(100), APDPSI(100),
      C PSILL(100), AREAN(100), PSILL(100), FRAC(100),
      C EQUIVALENCE (P(101), PSILL),
      C 1 P(201), AREAN, (P41001), PDCT, (P(1201), APDPSI),
      C 2 P(1301), PSILL, (P(1401), FRAC),
      C EQUIVALENCE (INTEGER(11), MPSILL), (INTEGER(12), MPSILL),
      C DELTA = PSILL(2) - PSILL(1)
      C DO 10 J = 1, MPSILL
      C   APDPSI(J) = 1.0 - PPSI(J)
      C   IF (AREAN(J) - APDPSI(J)) 20, 50, 50
      C   WRITE (6,30)
      C 20 FORMAT (10X, 4HEMQR MESSAGE - AREAN(1) LESS THAN APDPSI(1) )
      C   CALL PRINTR
      C   IF (AREAN(MPSILL) - APDPSI(MPSILL)) 40, 40, 40
      C   WRITE (6,70)
      C 40 FORMAT (10X, 5HEMQR MESSAGE - AREAN(MPSILL) GREATER THAN APDPSI(MPSILL) )
      C   CALL PRINTR
      C 50 CONTINUE
      C 100 PSILL(J) = PSILL(1)
      C 110 IF (1-1) 120, 120, 130
      C 120 P1 = APDPSI(J)
      C 130 P2 = APDPSI(J+1)
      C 140 P3 = APCPSI(13)
      C 150 GO TO 140
      C 160 P1 = APDPSI(J+1)
      C 170 P2 = APDPSI(J)
      C 180 P3 = APCPSI(11)
      C 190 A = 0.5 * P1 - P2 + 0.5 * P3
      C 200 B = -0.5 * P1 + 0.5 * P3
      C 210 C = P2 - AREAN(J)
      C 220 DISC = B * P2 + 4.0 * A * C
      C 230 IF (DISC) 142, 144, 144
      C 240 WRITE (6,143) DISC
      C 250 CALL PRINTR
      C 260 EIA = (1 - P + SORT(DISC)) / (2.0 * A)
      C 270 IF (1-1) 150, 150, 160
      C 280 PSILL(J) = PSILL(1) + EIA * DELTA
      C 290 GO TO 180
      C 300 PSILL(J) = PSILL(1) + EIA * DELTA
      C 310 GO TO 180
      C 320 CONTINUE
      C 330 CONTINUE
      C 340 NPR = MPSILL - 1
      C 350 FRAC(1) = (AREAN(1) + AREAN(2)) / 2.0
      C 360 DO 190 I = 2, NPR
      C 370 FRAC(I) = (AREAN(I+1) - AREAN(I-1)) / 2.0
      C 380 FRAC(MPSILL) = 1.0 - (AREAN(MPSILL) +
```


PAGE 2

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OPT-1

7474

SUBROUTINE LDLVL

1 AREANIMPSILL-101 / 2.0
RETURN
END

LDLV 458
LDLV 46
LDLV 47

60

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C      SUBROUTINE LDCOEFF
C      SUBROUTINE FOR COMPUTING THE LOAD CONDITION COEFFICIENTS
C      COMMON P(10000), MTEG(9100), TABL(2000,2),
C      1 TABL2(500,1)
C      DIMENSION PSILL(1000), PS(25,25), ALPHA(25),
C      1 PLOS(100,25), AINVS(50), AINVS(25,25), PLO(25)
C      EQUIVALENCE IF(301), PSI, (PIL301), PSILL,
C      1 (PIL501), PLOS, (PIL4001), ALPHA
C      EQUIVALENCE INTEGR(112), NPSTILL, (INTEGR(131), NPS),
C      1 (INTEGR(141), NPAGE), (INTEGR(150), NPSET)
C      NPSET = NPSET + 1
C      DO 10 I = 1, NPSTILL
C      10 PLOS(I,1) = PSILL(I)
C      IF (NPSET - NPS) 130, 20, 20
C      DO 50 I = 1, NPS
C      20 DO 50 J = 1, NPS
C      15 AII(J) = PS(I,J)
C      JNPS = J + NPS
C      IF (I - J) 40, 30, 40
C      30 AII(JNPS) = 1.0
C      GO TO 50
C      40 AII(JNPS) = 0.0
C      50 CONTINUE
C      CALL GAUSS21 (NPS, NPS, 1.0E-07, A, AINV, K3)
C      IF (K3 - 1) 60, 75, 60
C      25 WRITE (6,70) K3
C      60 FORMAT (10X, 24HGAUSS21 ERROR SIGNAL - K3 = , I3 )
C      70 NPAGE = NPAGE + 1
C      CALL PACFIN
C      DO 120 I = 1, NPSTILL
C      30 DO 80 J = 1, NPS
C      80 PLO(I,J) = PLOS(I,J)
C      DO 90 K = 1, NPS
C      35 DO 90 L = 1, NPS
C      90 ALPHA(K) = AINV(K,L) * PLO(I) + ALPHA(K)
C      100 WRITE (6,100) I
C      100 FORMAT (10X, 36HCOEFFICIENTS FOR FREQUENCY LEVEL NO. , I5 )
C      110 WRITE (6,110) (ALPHA(I), IA = 1, NPS)
C      120 FORMAT (1P8E12.6)
C      120 CONTINUE
C      130 RETURN
C      130 END

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SUBROUTINE PAGE NO. 2474 OPT=1 11/82/23 00-85-51. PAGE 1
SUBROUTINE FOR NUMBERING THE PAGES AND IDENTIFYING THE RUN
COMMON P10000, MYCER1000, TAIL4(2000,21),
1 TAIL2(500,1)
INTEGER DAY, YEAR
EQUIVALENCE (INTEGER(11), IDENT), (INTEGER(10), MONTH),
2 (INTEGER(10), DAY), (INTEGER(10), YEAR), (INTEGER(4), NPAGE)
WRITE (6,20) IDENT, MONTH, DAY, YEAR, NPAGE
20 FORMAT(11H1,9H,6HRUN NO, 16, 10X, 4HDATE, 16, 1H/, 12, 1H/, 14, NPAGE)
10 1 10X, 7HPAGE NO, 16 )
RETURN
END
PACH 1
PACH 2
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PACH 6
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PACH 8
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PACH 11
PACH 12
PACH 13
PACH 14

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SUBROUTINE GAUSS2 74/24 OPT=1 11/02/73 89.05.54 PAGE 1
      SUBROUTINE GAUSS2(M,EP,AT,KERN-
      DIMENSION A(3,4), X(3,1)
      NPM=N+M
      DO 34 L=1,N
      KP=0
      PD=0
      DO 12 K=1,M
      IF(17-ABS(A(K,L)))11,12,12
      Z=ALX(A(K,L))
      KPEX
      11 CONTINUE
      IF(L-KP)13,20,20
      DO 14 J=1,NPM
      Z=AL(J)
      AL(J)=AL(KP,J)
      14 AL(KP,J)=Z
      20 IF(L=5)15,11,11-EP)50,50,30
      IF(L-N)31,40,40
      LPI=L+1
      DO 34 K=LPI,N
      IF(L(K,L))32,34,32
      32 RPTID=AL(K,L)/AL(L,L)
      DO 33 J=LPI,NPM
      33 AL(K,J)=AL(K,J)-RATIO*AL(L,J)
      34 CONTINUE
      DO 43 L=1,N
      IF(L=1)1
      40 DO 43 J=1,M
      JN=J+N
      S=0.1
      IF(11-N)41,43,43
      41 IF(11)101
      DO 42 K=LPI,N
      S=S+AL(K)*X(K,J)
      42 X(K),J)=(AL(K,JN)-S)/A(11,11)
      43 K=1
      GO TO 75
      50 K=1
      75 CONTINUE
      RETURN
      END
      GAUS 001
      GAUS 2
      GAUS 003
      GAUS 004
      GAUS 005
      GAUS 006
      GAUS 007
      GAUS 008
      GAUS 009
      GAUS 010
      GAUS 011
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      GAUS 035
      GAUS 036
      GAUS 037
      GAUS 038
      GAUS 039
      GAUS 040

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| GAUSS | 001 | GAUSS | 002 |
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| GAUSS 001 | GAUSS 002 | GAUSS 003 | GAUSS 004 |
| GAUSS 005 | GAUSS 006 | GAUSS 007 | GAUSS 008 |
| GAUSS 009 | GAUSS 010 | GAUSS 011 | GAUSS 012 |
| GAUSS 013 | GAUSS 014 | GAUSS 015 | GAUSS 016 |
| GAUSS 017 | GAUSS 018 | GAUSS 019 | GAUSS 020 |
| GAUSS 021 | GAUSS 022 | GAUSS 023 | GAUSS 024 |
| GAUSS 025 | GAUSS 026 | GAUSS 027 | GAUSS 028 |
| GAUSS 029 | GAUSS 030 | GAUSS 031 | GAUSS 032 |
| GAUSS 033 | GAUSS 034 | GAUSS 035 | GAUSS 036 |
| GAUSS 037 | GAUSS 038 | GAUSS 039 | GAUSS 040 |
| GAUSS 041 | GAUSS 042 | GAUSS 043 | GAUSS 044 |
| GAUSS 045 | GAUSS 046 | GAUSS 047 | GAUSS 048 |
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| GAUSS 073 | GAUSS 074 | GAUSS 075 | GAUSS 076 |
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| GAUSS 197 | GAUSS 198 | GAUSS 199 | GAUSS 200 |

